



## Research articles

# Dynamic tuning by hydrostatic pressure of magnetocaloric properties to Ericsson like cycles

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## ARTICLE INFO

## ABSTRACT

A method to increase the relative cooling power to be used in Ericsson like refrigeration cycles is presented. The technique is based in the modification of the magnetic properties by the application of hydrostatic pressure on magnetic samples. The main advantage is to reach larger values of the magnetic entropy change in a wider temperature region (the so-called “table like” behavior). The study was carried out in a manganite belonging to the family of  $\text{La}_{0.625-y}\text{Nd}_y\text{Ca}_{0.375}\text{MnO}_3$ , and some conclusions were compared with the expected behavior in other materials extracted from literature.

## 1. Introduction

Magnetic refrigeration has been proposed as one of the most promising technologies to replace conventional refrigerators, which operate by gas compression-expansion cycles [1].

Refrigerators based in the use of the magnetocaloric effect (MCE), present a large number of benefits compared with gas based ones, providing a higher energy efficiency and avoiding the use of greenhouse gases.

The MCE has been widely used for cooling applications at low temperature taking advantage of the adiabatic demagnetization presented by many paramagnetic salts. However, the use of MCE in room temperature refrigeration is, at this moment, in experimental stage in research laboratories.

The observation of large MCE at room temperature in Gd based compounds, has motivated the scientific community to increase its efforts and a lot of research has been dedicated to the study to this particular topic seeking for a material with large MCE at room temperature and low cost of production. A large number of different families of compounds were proposed to replace Gd, such as As based compounds [2], heusler alloys [3],  $\text{LaFe}(\text{Si},\text{La})$  [4] and mixed-valence manganese oxides (manganites) [5].

Manganites were widely studied a decade ago due to the colossal magnetoresistance effect, a thousandfold reduction of the electrical resistivity that can potentially be used in magnetic reading heads and magnetic data storage devices. Besides, the magnetic properties of manganites can be easily tuned by different mechanisms, such as strain in thin films [6], grain size [7] and cation substitution [8]. This characteristic combined with the low cost of production

positioned to manganites as one of the plausible materials to be used in MCE applications.

The MCE can be quantified by the entropy change produced by the application of the magnetic field ( $\Delta S$ ), being its temperature dependence typically characterized by a peak around the transition temperature.

In order to manipulate the magnetocaloric properties of a system it is possible to apply a hydrostatic pressure on it. Depending of the system this can result in an enlargement of the entropy change [9–11] or in the modification of the transition temperature, resulting in a displacement of the temperature where the maximum entropy change is reached [12,13]. Even more, the use of pressure to induce or assist a magnetic transition has been proposed due to its proficiency to favor magnetic ordering [14].

The relative cooling power (RCP) defined as the product of the maximum entropy change and the temperature width of the peak is another magnitude to consider when a material is being analyzed [15]. A large RCP implies a large temperature range where the material will be suitable to produce an adequate cooling effect considering an Ericsson like cycle.

To increase the RCP some authors have proposed the use of cascade magnetic cycles [16]. To reach this they use magnetic systems with multiple magnetic transitions, composites [17,18] or layered structures [19] formed by materials with different transition temperatures. The primary objective of this kind of approach is to obtain an almost constant value of  $\Delta S$  in the working temperature range obtaining a “table-like” temperature dependence [20]. In that sense Paticopoulos and co-workers [21] studied different mixtures of  $\text{Fe}_{88-2y}\text{Co}_y\text{Ni}_y\text{Zr}_7\text{B}_4\text{Cu}_1$  alloys with  $y = 8.25$  and  $y = 11$ , obtaining the optimal proportion to reach an almost constant entropy change value in a larger temperature region. But, as the width of the entropy change is enlarged, the height is decreased

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when the entropy is normalized with the total mass of the composite. Because of that, the use of composites must be carefully evaluated for each refrigeration device as a particular case.

Gildas Diguët and co-workers analyzed the use of a composite magnetic material in a regeneration Ericsson refrigerator [22]. They used Gd, Gd<sub>0.74</sub>Tb<sub>0.26</sub> and (Gd<sub>3.5</sub>Tb<sub>1.5</sub>)Si<sub>4</sub> as the working materials and they conclude that use of the composite represents an improvement when it is compared with the performance of the separated components. The component were selected to obtain a satisfactory magnetocaloric behavior between T<sub>cold</sub> = 280 K and T<sub>hot</sub> = 300 K, meaning that ΔS presents an almost constant value in this temperature range.

In this work we will analyze the possibility to increase the RCP using the hydrostatic pressure as a “dynamic tuner” to reach a “table-like” entropy change dependence with temperature. We will discuss the application of the proposed method in composite samples and compare our results with those extracted from the literature.

## 2. Materials and methods

Ceramic samples of La<sub>0.425</sub>Nd<sub>0.20</sub>Ca<sub>0.375</sub>MnO<sub>3</sub> were obtained by liquid mix as it is described in reference [23]. Magnetization measurements as function of temperature and magnetic field were performed in a Quantum Design Versalab VSM magnetometer. High pressure measurements were obtained using a high pressure cell manufactured by HMD model CC-SPR-8.5-D-MC4-1.

## 3. Results and discussion

In Fig. 1 we present magnetization as function of temperature for the La<sub>0.425</sub>Nd<sub>0.20</sub>Ca<sub>0.375</sub>MnO<sub>3</sub> manganite for different applied magnetic fields (top) and hydrostatic pressure values (bottom). The sample presents a single magnetic transition from a paramagnetic insulator (PI) state at high temperature to a

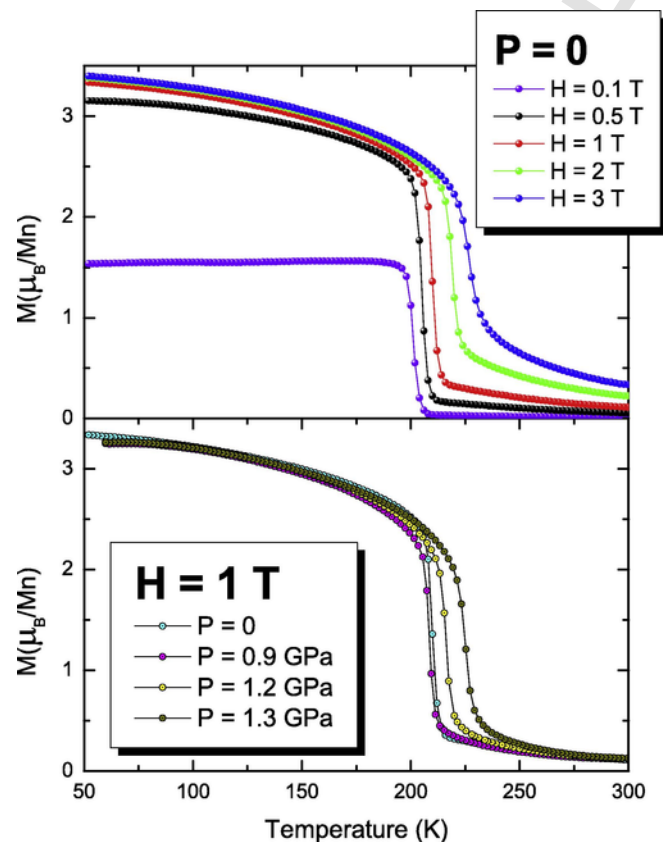


Fig. 1. magnetic moment as function of temperature at ambient pressure and different magnetic fields (top) and at a fixed field of 1 T and varying the hydrostatic pressure (bottom).

ferromagnetic metallic (FM) at low temperature. The transition temperature increases both by the application of the magnetic field and the hydrostatic pressure consistently with the behavior observed in similar systems [24,25].

In order to calculate the entropy change of the system we used the Maxwell relation

$$\Delta S(T, H) = \int_0^H \left( \frac{\partial M}{\partial T} \right)_{H'} dH' \quad (1)$$

The integral in Eq. (1) can be obtained from isothermal magnetization loops measured at small temperature intervals. In order to avoid an overestimation of the entropy change the sample was carried out to ambient temperature after each magnetization loop [26]. The temperature dependence of ΔS, obtained from Eq. (1), is presented in Fig. 2. In all cases the data presents a peak that can be characterized by three parameters: the maximum (ΔS<sub>MAX</sub>), the center (T<sub>MAX</sub>) and the width (quantified by the full width half maximum, δT<sub>FWHM</sub>). In Fig. 3 (top) we present the dependence of ΔS<sub>MAX</sub> and the δT<sub>FWHM</sub> with magnetic field. The value of the ΔS<sub>MAX</sub> increases with magnetic field, showing a clear tendency towards saturation at 7 J/KgK approximately. In contrast, no significant changes were observed with the application of hydrostatic pressure. In a similar way, the δT<sub>FWHM</sub> increases almost linearly with the magnetic field but does not show a clear dependence with the hydrostatic pressure.

It has to be noticed that it is not expected to observe a clear dependence of the RCP with the hydrostatic pressure, as neither ΔS<sub>MAX</sub> nor δT<sub>FWHM</sub> do.

For the case of T<sub>MAX</sub> we can observe that both H and P introduce a displacement of the center of the peak towards higher temperatures. This behavior is consistent with the temperature dependence of the magnetization presented in Fig. 1, where both H and P tend to favor ferromagnetic ordering, a fact that can be noticed in the increase of the PI to FM transition temperature.

If we assume a linear dependence of T<sub>MAX</sub> with H and P, it is possible to fit the center of the peak as  $T_{MAX}(H, P) = 198 K + 4 \frac{K}{T} H + 17 \frac{K}{GPa} P$ .

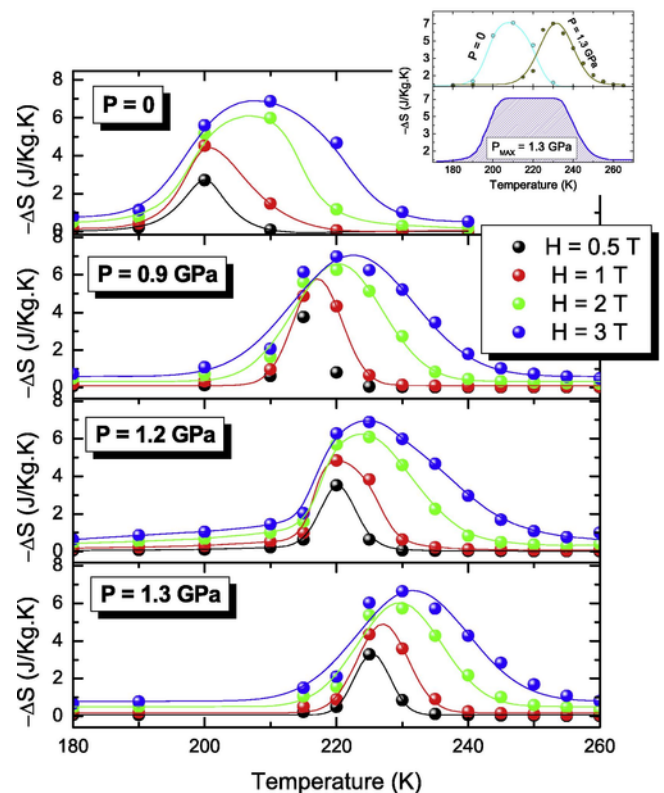


Fig. 2. Entropy change as function of temperature for different magnetic fields and hydrostatic pressure values. In the inset we show how the effective table like behavior can be obtained merging entropy curves with different applied pressure (the applied magnetic field was 3 T).

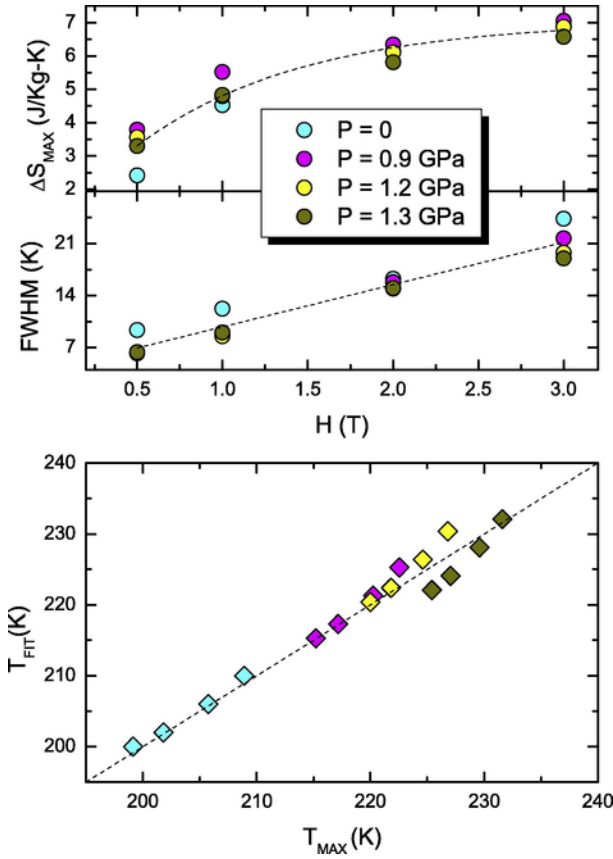


Fig. 3. (Top) Maximum and full width half maximum of the entropy change as function of the applied magnetic field. Colors indicate the value of the hydrostatic pressure. (Bottom) Comparison between the temperature of the center of the peak with the obtained from the proposed magnetic field and pressure dependence. (For interpretation of the references to colour in this figure legend, the reader is referred to the web version of this article.)

This fitting shows that an approximate “equivalence” between the magnetic field and hydrostatic pressure exists in this system. For example, the application of 1 GPa of hydrostatic pressure produces the same effect in  $T_{MAX}$  than the application of a 4 Tesla magnetic field.

The above presented results can be used to understand how the magnetic and magnetocaloric properties of this system can be tuned by the application of hydrostatic pressure. The center of the peak can be modified with no significant changes in  $\Delta S_{MAX}$  and  $\delta T_{FWHM}$ , which are mainly dominated by the magnetic field.

In an oversimplified point of view we can think that the application of hydrostatic pressure modifies the system giving place to a new sample with the same RCP but different  $T_{MAX}$ . This resembles the main motivation of the use of composites to obtain a “table-like” entropy change curve. The center of the

peak can be tuned in some temperature range by the application of  $P$ , depending on the requirements of the magnetocaloric device. Additionally, since the entire sample changes its properties, the efficiency remains unchanged due to the absence of “no-active” regions of sample. To quantify the effect of the application of the pressure in the magnetocaloric capacity we can introduce the *baromagnetocaloric cooling power* (BMCP) defined as

$$BMCP = \Delta S_{MAX} \cdot (\delta T_{FWHM} + \Delta T_C^p) \quad (2)$$

where  $\Delta S_{MAX}$  is the maximum entropy change,  $\delta T_{FWHM}$  is the full width half maximum of the peak and  $\Delta T_C^p$  is the change in the Curie temperature produced by the application of the hydrostatic pressure.

This quantity can be expressed in terms of the RCP and the rate of change of  $T_C$  as

$$BMCP = RCP \cdot \left( 1 + \frac{dT_C}{dP} \frac{P_{MAX}}{\delta T_{FWHM}} \right) \quad (3)$$

$P_{MAX}$  is the largest pressure that can be applied and is related with the design of the magnetocaloric device.

In Table 1 we present the values of BMCP relative to the RCP for the  $\text{La}_{0.425}\text{Nd}_{0.20}\text{Ca}_{0.375}\text{MnO}_3$  sample and for different systems of the literature, considering  $P_{MAX} = 1$  GPa.

The value of BMCP can be considered the RCP of a new “virtual” material in which its cooling capacities are extended by the application of the external pressure. It is interesting to note how BMCP becomes larger in those systems where the application of pressure produces an important change in the transition temperature (i.e.  $\text{LaFe}_{11.6}\text{Si}_{1.4}$ ). In that sense, the compound  $\text{La}_{0.425}\text{Nd}_{0.20}\text{Ca}_{0.375}\text{MnO}_3$  is far for being the most reliable choice for this kind of applications, but is a good example to understand our approach.

The main advantage of this approach compared with the use of composites of materials is the absence of efficiency decrease, since the entire sample will be “active” during the application of the magnetic field in the Ericsson like cycle. The obvious disadvantage is the additional complexity in a refrigeration device due to the necessity to control the external pressure. The design of the refrigeration device will include some kind of feedback in order to improve the efficiency of the entire process.

#### 4. Conclusions

Summarizing, we have analyzed the influence of hydrostatic pressure in magnetic samples of  $\text{La}_{0.425}\text{Nd}_{0.20}\text{Ca}_{0.375}\text{MnO}_3$  focusing our attention in those parameters that characterize the magnetocaloric effect (i.e. entropy change and relative cooling power). The application of pressure provokes an increase in the ferromagnetic transition temperature in a ratio of 17K/GPa, keeping the maximum entropy change almost invariant at 7J/kg-K (for a magnetic field of 3T). Based on this behavior, we propose the use of pressure to tune the transition temperature as an alternative path (as compared with the use of composites or similar methods) to obtain a “table-like” temperature dependence in the entropy change.

Table 1

Compound	dTc/dP [K/GPa]	DSmax [J/kg-K]	R. C. P [J/kg]	BMCP/RCP	Ref.
$\text{La}_{0.425}\text{Nd}_{0.20}\text{Ca}_{0.375}\text{MnO}_3$	17	7	150	1.5	Present work
$\text{Pr}_{0.6}\text{Ca}_{0.4}\text{Mn}_{0.96}\text{Co}_{0.04}\text{O}_3$	34.1	7 (P = 0)4.5 (P = .91 GPa)	150	2.7	18
$\text{Pr}_{0.6}\text{Ca}_{0.4}\text{Mn}_{0.96}\text{Cr}_{0.04}\text{O}_3$	31.1	5 (P = 0)3.5 (P = 0.95)	170	1.91	18
$\text{La}_{0.8}\text{Sr}_{0.2}\text{MnO}_3$	15	6.5 (P = 0)6 (P = .67 GPa)	230	1.45	19
$\text{La}_{0.69}\text{Ca}_{0.31}\text{MnO}_3$	21.4	7	140	2	20
$\text{LaFe}_{11.6}\text{Si}_{1.4}$	130	10 (P = 0)40 (P = .83)	50 (P = 0)200 (P = .83)	27	9
$\text{Tb}_5\text{Si}_2\text{Ge}_2$	5.3	13.4	268	1.265	10

To quantify this improvement we have introduced the “baromagneto-caloric cooling power”, which takes into account the magnetocaloric response of the system and the “tuneability” of the magnetic transition temperature. We used BMCP to quantify the effect in other systems reported in literature, obtaining a significant increase in all cases.

Even when the application of this particular approach implies an improvement in the cooling capacity, its practical implementation is still challenging, as the application of hydrostatic pressure in a practical device is far from being simple.

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