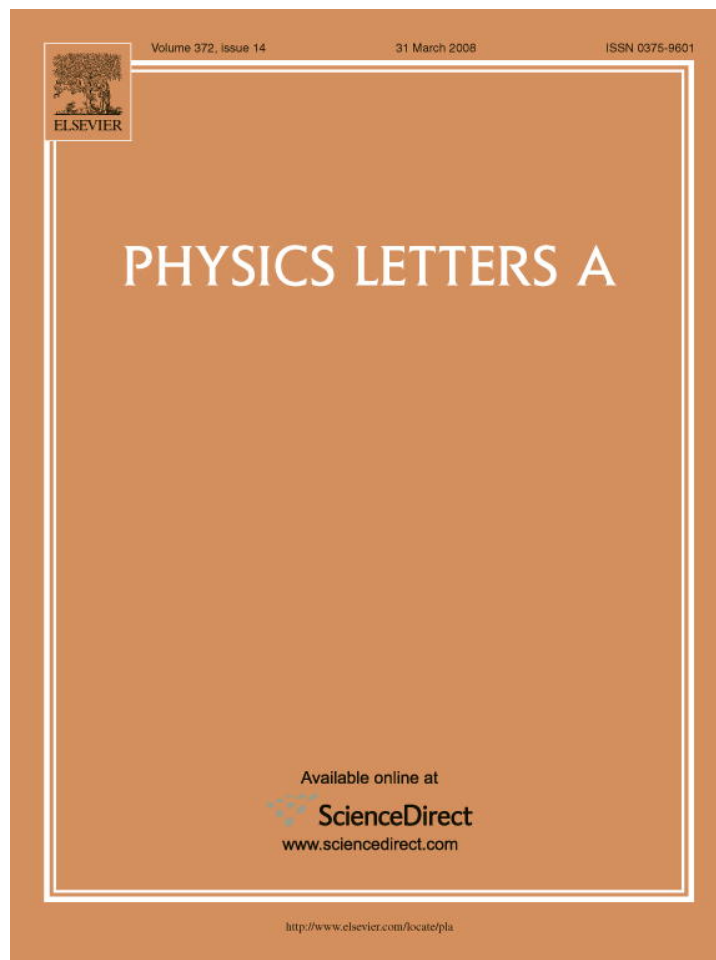


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On metallic gratings coated conformally with isotropic negative-phase-velocity materials

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Abstract

Application of the differential method (also called the C method) to plane-wave diffraction by a perfectly conducting, sinusoidally corrugated metallic grating coated with a linear, homogeneous, isotropic, lossless dielectric–magnetic material shows that coating materials with negative index of refraction may deliver enhanced maximum nonspecular reflection efficiencies in comparison to coating materials with positive index of refraction.

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1. Introduction

Surface–relief gratings are commonly made of metals. Often, dielectric coatings are deposited on top of such gratings for protection against environmental degradation as well as to increase the reflection efficiency (which is the same as the specular reflectance) [1,2]. Thus, a coated grating is a dielectric slab sitting atop a periodically corrugated metallic surface. Various different types of dielectric coatings have been examined, ranging from conformal coatings to coatings that simply fill up the grooves of the gratings [3–5].

The recent emergence of electromagnetic metamaterials [6] has opened new avenues. Meta-material coatings could be employed for tailoring the specular and the nonspecular re-

flectances of metallic gratings. Specifically, metamaterials wherein the time-averaged Poynting vector is in opposition to the phase velocity are very attractive [7,8]. Indeed, gratings made of isotropic negative-phase-velocity (NPV) materials have been analytically investigated already [9–11], and numerical results show that they function very differently from their positive-phase-velocity (PPV) analogs.

The focus of this communication is on sinusoidally corrugated metallic gratings with conformal coatings of constant thickness made of homogeneous, isotropic NPV materials. The differential or the C method [12–15] was adapted for that purpose. A comparison of NPV and PPV coating materials in relation to specular and nonspecular reflection efficiencies was undertaken.

2. Diffraction problem

Let us consider plane wave diffraction from a coated perfectly conducting grating illuminated by a plane wave. The geometry of the diffraction problem is shown in Fig. 1. The region of incidence and reflection $y > y_2(x)$ is vacuous. The coat-

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ing region $y_1(x) < y < y_2(x)$ is filled by a linear, homogeneous, isotropic, lossless dielectric–magnetic material characterized by relative permittivity ϵ_r and relative permeability μ_r . The grating surface $y = y_1(x)$ is periodic such that $y_1(x \pm d) = y_1(x)$ with d as the period, and the coating thickness D is uniform so that $y_2(x) = y_1(x) + D$. The grooves of the grating are along the z axis. A linearly polarized electromagnetic plane wave of angular frequency ω is incident from the vacuous region at an angle θ_0 with respect to the y axis, with the plane of incidence being the xy plane. An $\exp(-i\omega t)$ dependence on time t is implicit here.

Due to a perfectly conducting flat surface coated with a uniform, lossless PPV material, the reflection is completely specular and the specular reflectance possesses a magnitude of unity. If the signs of ϵ_r and μ_r are changed, the reflection is still specular, the magnitude of the specular reflectance still remains unity, but the phase of the reflection coefficient changes [16].

When the perfectly conducting surface is corrugated periodically, nonspecular modes must arise in the reflected field. The characteristics of these modes will depend, in principle, on whether the coating material is of the PPV or of the NPV type. In accordance with the focus of this communication, we must investigate two cases. With the definition of the refractive index

$$n = \sqrt{\epsilon_r} \sqrt{\mu_r}, \quad (1)$$

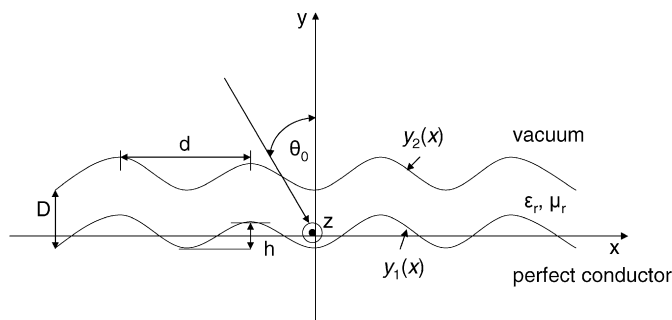
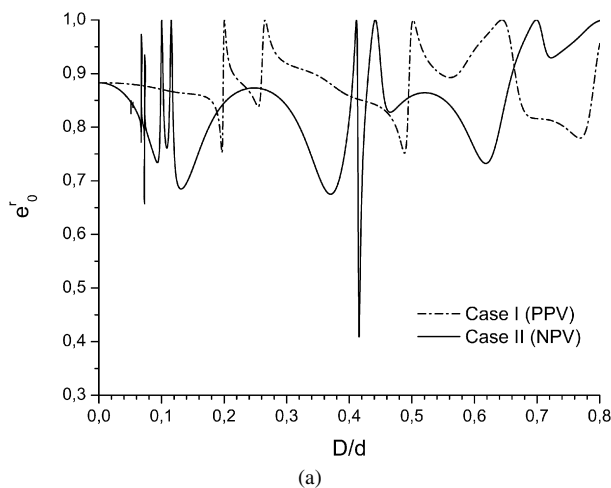


Fig. 1. Geometry of the diffraction problem.



wherein the right side must not be confused with $\sqrt{\epsilon_r \mu_r}$, these two cases are as follows:

- I. $n > 0$, i.e., the coating material is of the PPV type;
- II. $n < 0$, i.e., the coating material is of the NPV type.

As mentioned in the previous section, we used a computer code based on the differential or the C method, the details of which are available elsewhere [12–15]. This code yielded the reflection coefficients r_m ($m = 0, \pm 1, \pm 2, \dots$), wherefrom the reflection efficiencies e_m^r were computed [15, Eq. 28] for the specular ($m = 0$) and the nonspecular ($m \neq 0$) of the reflected field. Although our computational method is suitable for grooves of arbitrary shape, we chose to restrict our attention here to sinusoidal gratings; i.e.,

$$y_1(x) = 0.5h \cos\left(\frac{2\pi x}{d}\right) \quad (2)$$

where h is the groove depth.

3. Numerical results and discussion

Calculations were made for the following constitutive parameters of the coating material:

Case I: $\{\epsilon_r = 2.5, \mu_r = 1.2\} \Rightarrow n = 1.732$;

Case II: $\{\epsilon_r = -2.5, \mu_r = -1.2\} \Rightarrow n = -1.732$.

Both linear polarization states—parallel (p) and perpendicular (s)—of the incident plane wave.

Let us begin with the specular reflection efficiencies e_0^r calculated as functions of the normalized coating thickness D/d , when the angle of incidence $\theta_0 = 30^\circ$, the free-space wavelength $\lambda = 0.81d$, and the groove depth $h = 0.1d$. As may be gleaned from Fig. 2, the specular reflection efficiencies are significantly affected by the type of the coating material. In particular, for the PPV coating material and for both s and p polarization states, the specular reflection efficiencies are high: more than 70% of the energy incident onto the grating for the

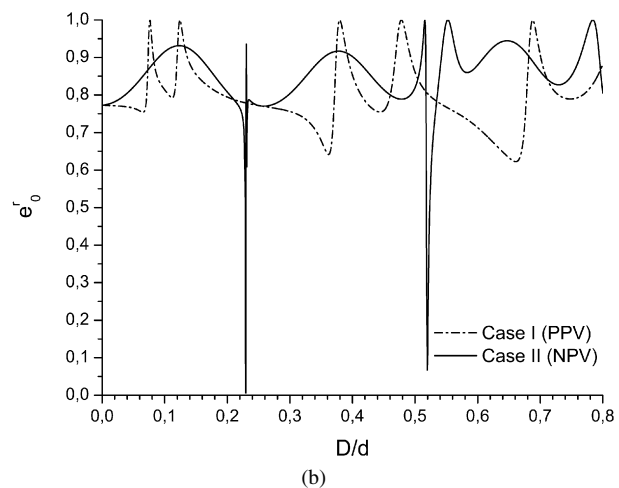


Fig. 2. Specular reflection efficiencies e_0^r vs. normalized thickness D/d of the coating, when $\theta_0 = 30^\circ$, $\lambda = 0.81d$, and $h = 0.1d$. (a) s polarization state, (b) p polarization state.

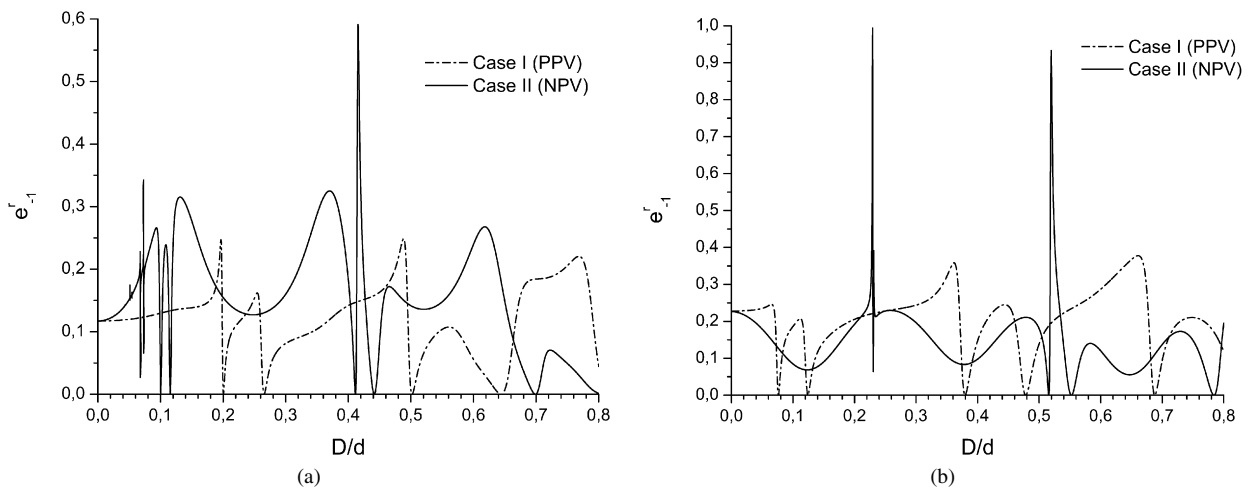


Fig. 3. Same as Fig. 2, but for e_{-1}^r .

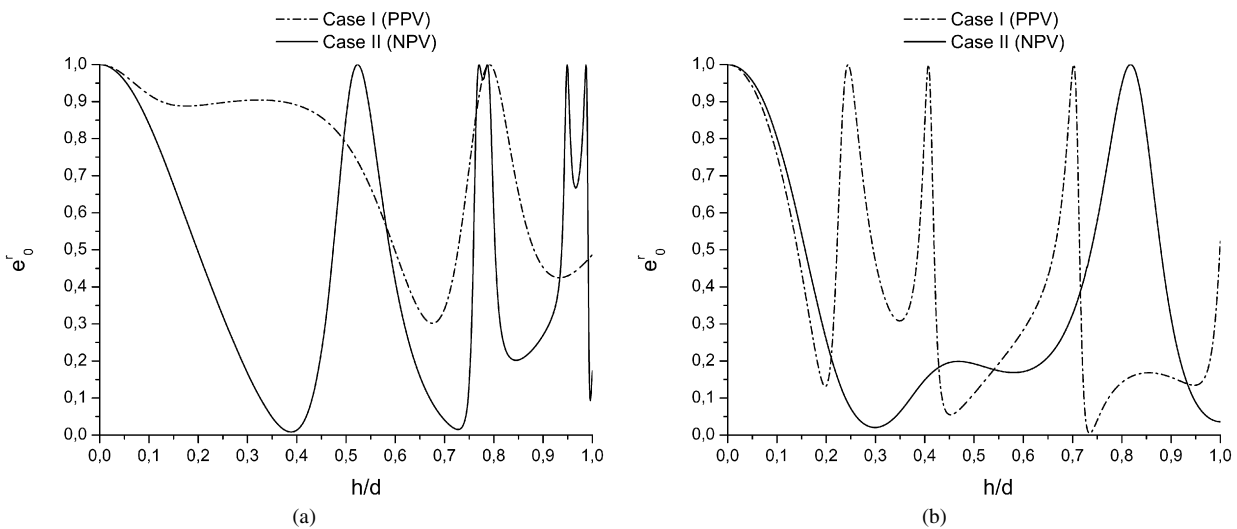


Fig. 4. Specular reflection efficiencies e_0^r vs. normalized groove depth h/d of the coating, when $\theta_0 = 30^\circ$, $\lambda = 0.81d$, and $D = 0.3d$. (a) s polarization state, (b) p polarization state.

s polarization state, and more than 60% for the p polarization state, is reflected specularly. Narrow dips appear at certain values of D/d , at which the value of the specular reflection efficiency decreases to a minimum value between 0.62 and 0.75, for both incident polarization states. Although the specular reflection efficiencies are also high for the NPV coating material, the plots exhibit more pronounced dips. For example, the value of e_0^r decreases abruptly for the s polarization state, reaching a minimum value of about 0.4 for $D/d \sim 0.42$; for the p polarization state, two dips appear at $D/d \sim 0.22$ and $D/d \sim 0.52$, the specular reflection efficiency decreasing to about 0 and 0.1, respectively.

When the value of e_0^r dips, an enhancement of the energy carried by the $m = -1$ reflected order appears for both types of coating materials. However, the reflection of power into this order for the NPV coating material is much larger than for the PPV coating material, a fact that can be appreciated in Fig. 3, wherein e_{-1}^r is plotted against D/d for both polarization states and the same parameters as for Fig. 2. The increased maximum nonspecular reflection efficiencies represent an im-

portant distinction between the PPV and NPV coating materials.

Next we present the specular reflection efficiencies e_0^r in Fig. 4 as functions of the normalized groove depth h/d when the normalized coating thickness $D/d = 0.3$, but the other parameters are the same as for Fig. 2. Let us begin analyzing the results for the s polarization state presented in Fig. 4(a). For the PPV coating material and for $h/d < 0.4$, e_0^r does not vary significantly. However, for deeper grooves, the value of the specular reflection efficiency depends strongly on h/d : it first decreases to a minimum value of about 0.3 for $h/d \approx 0.67$, then increases to unity, and then decreases again. In contrast, for the NPV coating materials, significant fluctuations in the value of e_0^r are observed for the entire range of h/d : $e_0^r \approx 0$ for certain values of h/d ($\approx 0.38, 0.72$), whereas $e_0^r \approx 1$ for other values of h/d (e.g., $h/d \approx 0.52$).

The e_0^r vs. h/d plots for the p polarization state in Fig. 4(b) are completely different from those for the s polarization state in Fig. 4(a). The plot for the PPV coating material in Fig. 4(b) is qualitatively similar to the one for the NPV coating material in

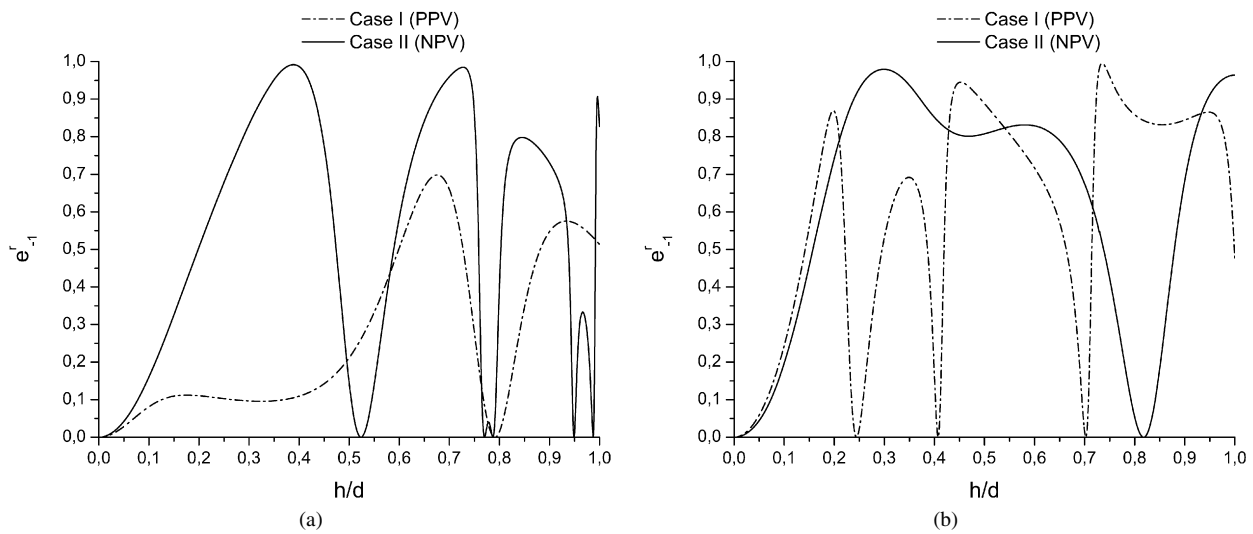


Fig. 5. Same as Fig. 4, but for e_{-1}^r .

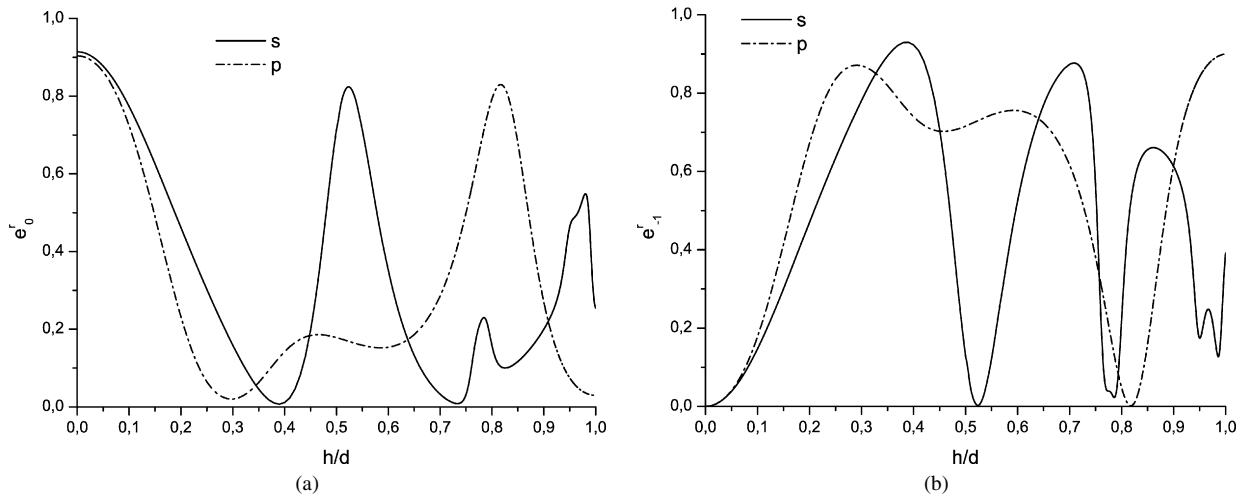


Fig. 6. Reflection efficiencies vs. normalized groove depth h/d of the coating, when $\epsilon_r = -2.5 + i0.01$, $\mu_r = -1.2 + i0.01$, $\theta_0 = 30^\circ$, $\lambda = 0.81d$, and $D = 0.3d$. (a) e_0^r , (b) e_{-1}^r .

Fig. 4(a): large variations in the value of the specular reflection efficiency can be appreciated in the two plots. Conversely, for the NPV coating, the specular reflection efficiency in Fig. 4(b) is generally quite low, except in the limit of the grating grooves becoming planar or when $h/d \approx 0.81$, where the entire incident energy is specularly reflected. In Fig. 5, the nonspecular efficiencies of the $m = -1$ reflected order are plotted as functions of h/d for the same parameters as for Fig. 4. An enhancement of the energy carried by the nonspecularly reflected order appears for both types of coating materials.

All known NPV materials are both dispersive and absorptive. Dispersion is irrelevant to this Letter, as we have considered only a single frequency. In order to identify the possible influence of weak absorption, we set $e_r = -2.5 + i0.01$ and $\mu_r = -1.2 + i0.01$ for the NPV coating material, and computed the reflection efficiencies e_0^r and e_{-1}^r for both polarization states as functions of the normalized groove depth h/d , when $D/d = 0.3$, $\lambda/d = 0.81$, and $\theta_0 = 30^\circ$. Fig. 6 contains the resulting curves. These are very similar to those for Case II in

Figs. 4 and 5 except the efficiencies are somewhat lower. Thus, the introduction of weak absorption in the NPV coating material is not likely to have a significant effect on the performance of the coated grating.

4. Conclusion

Using a rigorous electromagnetic method, we investigated the response of conformally coated, perfectly conducting, sinusoidal gratings. We considered transparent coatings and focused on the different responses obtained when the refractive index of the coating material is transformed from positive to negative. Our numerical results show that this transformation may have a significant influence on the diffraction efficiencies, a result that indicates that the emergence of homogeneous NPV materials promises new types of grating coatings which could be significantly different from their PPV counterparts. More specifically, coating materials with negative index of refraction may deliver enhanced maximum nonspecular reflection efficiencies in com-

parison to coating materials with positive index of refraction. Let us, however, caution that the foregoing conclusion requires confirmation by a comprehensive investigation that we shall undertake next.

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