¹ **Area law for magnetic domain walls in bent cylindrical nanowires**

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 The dynamics of several systems in nature occurs under some constraints and symmetries that ensure the appearance of constants of motion. In this work, we discuss the dynamics of the magnetic domain wall (DW) under the Walker regime (i.e., when its position oscillates as a function of time) in bent cylindrical magnetic nanowires (NWs) with constant curvatures. It is shown that the DW position sweeps, in relation to the curvature center, the same area for different NW curvatures. This phenomenon appears due to an exchange-driven curvature-induced interaction. The translational DW motion is accompanied by its rotation around the NW axis, leading to a periodic curvature-independent angular momentum, from which one obtains an area's law for the DW motion.

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¹⁷ **I. INTRODUCTION**

 Magnetic nanowires (NW) are nanostructures mimicking 19 one-dimensional systems $[1-3]$. They have exhibited many extremely interesting phenomena [\[4–6\]](#page-4-0), becoming a funda- mental pillar for the next generation of applications at the nanoscale [\[7–14\]](#page-4-0). Among them, the possibility of tuning do- main wall (DW) dynamics is probably the most attractive one from a technological perspective and consequently, a great deal of effort has been put in this direction $[15-17]$. During this undertaking, various unexpected and intriguing magnetic phenomena were reported on noncurved NWs (or nanos- tripes). For instance, a current-induced spin wave frequency 29 shift was identified as a Doppler effect $[18]$, an analogy of the Cherenkov radiation was found in magnetic domain walls emitting spin waves while moving sufficiently fast [\[19\]](#page-4-0), or the DW width contraction for velocities close to the spin wave group velocity was shown to obey similar laws to that of the special relativity $[20,21]$. These examples evidence the exis- tence of a plethora of interesting phenomena to be revealed in nanomagnetism.

37 Within the aim of tuning DW dynamics, the understand- ing of curvature-induced phenomena in magnetic NWs is an 39 important topic in current magnetism research [\[22\]](#page-4-0). Curva- ture induces a drastic change in the role that the exchange interaction plays in DW dynamics, leading to the appearance 42 of several interesting magnetic effects $[23-31]$ $[23-31]$. Among them, we can highlight the oscillatory behavior of the DW along the NW axis, similar to that corresponding to the Walker regime in straight NWs. It appears above a certain threshold for the external stimuli and reduces the DW average velocity in consonance with the Walker breakdown in faceted straight 48 NWs [\[15\]](#page-4-0). Nevertheless, in contrast to their noncurved coun- terpart [\[32\]](#page-5-0), this oscillatory behavior appears even for the case 50 of circular cross-section NWs [\[26\]](#page-5-0). The Walker breakdown threshold field results to be proportional to the NW curvature $\frac{51}{100}$ $[25,26]$ $[25,26]$.

In this work we demonstrate that, for the specific case $\frac{53}{2}$ of bent cylindrical NWs with constant curvature and un- ⁵⁴ der external magnetic fields within the Walker regime, the 55 previously reported translational and rotational DW motions 56 $[26,27]$ yield a time-periodic curvature-independent angular 57 momentum. This fact implies that the area covered by the DW 58 when "orbiting" around the curvature center of the NW is curvature independent but exhibits a periodic time dependence. $\frac{60}{2}$ The problem is presented in Fig. [1](#page-1-0) (based on our simulation 61 results to be discussed below), illustrating the area law for the $\frac{62}{2}$ DW dynamics in bent NWs, where the DW sweeps equal areas 63 in equal times, independent of the NW curvature. 64

II. MODEL AND RESULTS 65

To evidence the above statement, we analytically address 66 the problem, corroborating our results by using micromag- 67 netic simulations (using the finite-element software NMAG 68 $[33]$). Bent NWs with constant curvature are fully described $\frac{1}{69}$ as toroidal sections with a fixed length $\ell = 1 \mu m$, major π radius *R*, minor radius $a = 15$ nm, and opening angle ψ . τ_1 The relationship among these parameters is $\ell = \psi R$. The 72 curvature is defined as $\kappa = 1/R$. In analytical calculations, τ_3 *R* is a free parameter. The set of bent NWs considered in $_{74}$ micromagnetic simulations is described as $\ell = \frac{2\pi R_n}{n}$, where 75 $n \in [2, 10]$ is an integer number determining R_n , $\kappa_n = 1/R_n$, 76 and $\psi_n = 2\pi / n$.

The magnetization inside the NW can be parameterized using the local coordinate basis, $\mathbf{m} = \sin \Omega \sin \phi \hat{r} + \cos \Omega \hat{\theta} + \mathbf{v}$ $\sin \Omega \cos \phi \hat{z}$ (see Fig. [2\)](#page-1-0), where M_s and $\mathbf{m} = \mathbf{M}/M_s$ are the 80 saturation and normalized magnetization, respectively. Mag- 81 netic NWs exhibit transverse DWs (T_{dw}) up to a critical 82 diameter $D_{CR}(M_s)$ [\[34\]](#page-5-0). In this work the diameter of the NWs \quad 83

FIG. 1. Schematic representation of the area (shady regions) covered by a head-to-head transverse DW (T_{dw}) obtained from simulations for three concentric bent cylindrical nanowires with different curvatures. The sphere depicts the center of curvature for all wires. White arrows represent the applied azimuthal magnetic field with the same strength for all the NW. The magnetization is colored following its m_X component which corresponds to the in-plane vertical direction. R_2 , R_3 , and R_4 represent three different curvature radii.

84 is below this critical value, therefore we assume the existence 85 of transversal domain walls, T_{dw} . The following ansatz is 86 used for describing the T_{dw} profile: $\Omega = 2 \arctan{\exp[R(\theta - \theta)]}$ θ_0)]/ δ }, where $R\theta_0$ defines the position of the DW center, 88 and $\delta = \delta_W / \pi$ is the DW width (δ_W) divided by π . For our 89 calculations, the T_{dw} is considered a rigid body, with constant ⁹⁰ shape and size. Our micromagnetic simulations support this 91 approach. Thus, the DW dynamics can be described by the 92 position of its center and its phase $[\phi(t)]$.

FIG. 2. (a) Domain wall profile, and local and global coordinate bases used in this work. (b) NW orientation in the Cartesian reference system and geometric parameters.

The time evolution of the magnetization is given by the 93 Landau-Lifshitz-Gilbert (LLG) equation

$$
\frac{\partial \mathbf{M}}{\partial t} = -\gamma \mathbf{M} \times \mathbf{H}_{\text{eff}} + \frac{\alpha}{M_s} \mathbf{M} \times \frac{\partial \mathbf{M}}{\partial t},
$$
 (1)

where γ is the gyromagnetic ratio, α is the Gilbert damp- 95 ing parameter, and H_{eff} is the effective field coming from 96 the magnetostatic, exchange, Zeeman, and anisotropy interac-

⁹⁷ tions. The magnetostatic effective field is obtained from the 98 demagnetizing tensors, considering that the DW lies in an 99 ellipsoid inside the NW. In this case, $H_d = -4\pi (N_r M_r \hat{r} + 100$ $N_{\theta}M_{\theta}\hat{\theta} + N_zM_z\hat{z}$, where N_r , N_{θ} , and N_z are the demagnetizing factors along the \hat{r} , $\hat{\theta}$, and \hat{z} directions, respectively. 102 The exchange field is $\mathbf{H}_x = (2A/M_s)\nabla^2\mathbf{m}$. For simplicity, the 103 external magnetic field has a constant strength of $H = 11$ mT, 104 and is chosen tangent to the NW, i.e., $H_Z = H \hat{\theta}$ (see white 105 arrows in Fig 1). The field strength ensures that the DW $_{106}$ dynamics occurs under the Walker regime $[26]$. An azimuthal 107 magnetic field can be experimentally addressed, for instance, 108 from an electric current flowing perpendicular to the plane the ¹⁰⁹ bent NW forms. The magnetic parameters used in this work 110 correspond to that of Permalloy, that is, the exchange stiffness 111 and saturation magnetization are $A = 1.3 \times 10^{-11}$ J m⁻¹ and ¹¹² $M_s = 7.95 \times 10^5$ A m⁻¹, respectively. Permalloy does not 113 exhibit magnetocrystalline anisotropy. The domain wall width 114 for a cylindrical Permalloy NW with diameter $d = 30$ nm 115 is $\delta_W = 37$ nm [\[34\]](#page-5-0). Finally, we use the damping parameter 116 $\alpha = 0.01.$ 117

The DW dynamics is determined from the total torque Γ 118 evaluated on the DW center. Specifically, the total torque cor-
119 responds to that produced by the effective field ($\Gamma_{\text{eff}} = M \times 120$ **H**_{eff}) in addition to the one coming from the damping term. 121 The torques corresponding to the external magnetic field and 122 the damping are straightforwardly obtained, resulting in $\Gamma_H =$ 123 $M_s H(-\cos\phi \hat{r} + \sin\phi \hat{z})$ and $\Gamma_\alpha = -(\alpha M_s/\gamma)(\Omega \cos\phi \hat{r} + \omega^2)$ $\dot{\phi}$ $\hat{\theta}$ – $\dot{\Omega}$ sen ϕ \hat{z}), respectively. The torque originated from 125 the dipolar effective field in the DW center is evaluated as 126 $\Gamma_d = -2\pi M_s^2 \Delta N \text{sen}(2\phi) \hat{\theta}$, where $\Delta N = N_r - N_z$ [\[28\]](#page-5-0). For 127 NWs with a circular cross section one obtains $\Delta N = 0$ and 128

therefore, $\Gamma_d = 0$. Finally, for bent one-dimensional (1D) ¹³⁰ systems, the most important term in the total torque on the ¹³¹ DW consists of that produced by the exchange field, given by *i*₃₂ $\Gamma_x = A(\frac{4\cos\phi}{R^3} - \frac{\sin(2\phi)}{R^2})\hat{\theta}$. Under the above assumptions, the ¹³³ total torque can be written as

$$
\Gamma_{r,\theta,z} = \begin{bmatrix} -M_s \cos \phi \left(\frac{\alpha}{\gamma} \frac{d\Omega}{dt} + H \right) \\ -\frac{\alpha M_s}{\gamma} \frac{d\phi}{dt} + A \left(\frac{4 \cos \phi}{R\delta} - \frac{\sin(2\phi)}{R^2} \right) \\ M_s \sin \phi \left(\frac{\alpha}{\gamma} \frac{d\Omega}{dt} + H \right) \end{bmatrix} . \tag{2}
$$

¹³⁴ To simplify our analysis, it is convenient to rewrite the ¹³⁵ total torque in the local system of cylindrical coordinates (see Fig. [2\)](#page-1-0) as $\Gamma_{\rho, \Omega, \phi} = \mathcal{R} \Gamma_{r, \theta, z}$, where \mathcal{R} is the rotation matrix 137 that connects the two considered coordinate systems and $\hat{\rho}$ is ¹³⁸ a unitary radial vector. In this case, we obtain

$$
\Gamma_{\rho,\Omega,\phi} = \begin{bmatrix} 0 \\ \frac{\alpha M_s}{\gamma} \frac{d\phi}{dt} - A\left(\frac{4}{R\delta}\cos\phi - \frac{1}{R^2}\sin(2\phi)\right) \\ -M_s\left(\frac{\alpha}{\gamma} \frac{d\Omega}{dt} + H\right) \end{bmatrix} . \tag{3}
$$

¹³⁹ The substitution of the above expressions for the torques 140 reduces the LLG [Eq. (1)] to the following system of equa-¹⁴¹ tions for the two angles describing the DW center [see 142 Fig. $2(a)$]:

$$
\frac{d\phi}{dt} = -\frac{\gamma}{M_s} \Gamma_{\phi} \quad \text{and} \quad \frac{d\Omega}{dt} = -\frac{\gamma}{M_s} \Gamma_{\Omega} \,. \tag{4}
$$

143 Since we are evaluating the dynamics of the DW center, the linear velocity can be defined as $v = Rd\theta_0/dt = -\delta d\Omega/dt$. Therefore, after some algebra, it is possible to write the above set of equations in terms of the torque components. In this context, we obtain a system of coupled equations defining the DW velocity and phase as

$$
v(t) = \frac{\gamma}{1 + \alpha^2} \left[\alpha \delta H - \frac{A}{M_s R} \left(4 \cos \phi - \frac{\delta}{R} \sin(2\phi) \right) \right] (5)
$$

$$
\frac{d\phi}{dt} = \frac{\gamma}{1 + \alpha^2} \left[H + \frac{\alpha A}{M_s R \delta} \left(4 \cos \phi - \frac{\delta}{R} \sin(2\phi) \right) \right].
$$
 (6)

149 All the geometries considered in this work fulfill that $R \gg$ ¹⁵⁰ δ. Thus, terms proportional to δ/*R* in the above equations can ¹⁵¹ be neglected. Therefore, we obtain

$$
v(t) \approx \frac{\gamma \delta \alpha}{(1 + \alpha^2)} \left(H - \frac{4A}{RM_s \delta \alpha} \cos \phi \right) \tag{7}
$$

¹⁵² and

$$
\frac{d\phi}{dt} \approx \frac{\gamma}{1+\alpha^2} \left(H + \frac{4\alpha A}{M_s R \delta} \cos \phi \right). \tag{8}
$$

153 The initial condition for the integration is $\phi(0) = \pi/2$ ¹⁵⁴ (schematically displayed in Fig. [2\)](#page-1-0). That initial condition cor-155 responds to the equilibrium state of a head-to-head T_{dw} in bent ¹⁵⁶ cylindrical nanowires [\[23\]](#page-4-0) and matches with that obtained in ¹⁵⁷ our micromagnetic simulations.

Importantly, the term $\frac{4\alpha A}{RM\delta} \approx 0.1$ mT is two orders of mag-
158 **RMS** intude smaller than the external annlied field. Therefore, the nitude smaller than the external applied field. Therefore, the ¹⁶⁰ Walker regime is obtained even for smaller external stimuli

than the one considered here since the condition $\frac{4\alpha A}{RM_S\delta H} \ll 1$ 161 holds. In Eq. (7) the damping parameters are in the denominator and thus the first term is relatively small with respect to the $_{163}$ second one. Note that even without disregarding the second 164 term, Eq. (8) can be integrated to yield 165

$$
\phi(t) = 2 \arctan[\eta \tanh(\omega t + \arctanh(\xi))], \tag{9}
$$

where $\eta = \sqrt{\frac{H_W + H}{H_W - H}}, \xi = \sqrt{\frac{H_W - H}{H_W + H}}, \omega = \frac{\gamma}{2}$ $\frac{\sqrt{H_{W}^2 - H^2}}{1+\alpha^2}$, and the 166 Walker field is $H_W = \frac{4\alpha A}{RM_s\delta}$. In the limit $\frac{4\alpha A}{RM_s\delta H} \ll 1$ we obtain 167

$$
\phi(t) \approx \frac{\gamma H t}{1 + \alpha^2} + \frac{\pi}{2}.
$$

The analytical results for the DW velocity, obtained by 168 the integration of Eqs. (7) and (8), are presented in Fig. $3(a)$, 169 together with the direct micromagnetic simulations for three 170 different curvatures (κ_n) . The values of the velocity amplitude (V_{AMP}) are highlighted with dashed lines and labeled on 172 the right axis. Clearly, the velocity amplitude increases as a 173 function of the NW curvature. An interesting point is that the 174 amplitude of the velocity in Eq. (7) is field independent while 175 its frequency is not. 176

Figure $3(b)$ presents numerical and analytical results for 177 the DW velocity amplitudes as a function of the NW cur- ¹⁷⁸ vature. Our results evidence a linear dependence between 179 velocity and curvature. Importantly, the slope of the lines in 180 Fig. $3(b)$, obtained either by a linear fit (orange line) to the 181 numerical results (red circles) or by the analytical data (blue 182 line), have physical units of $m^2 s^{-1}$. Therefore, Fig. [3\(b\)](#page-3-0) sug- 183 gests the existence of an area covered in a certain amount of 184 time which is independent of the NW curvature. This finding 185 also directly follows from the fact that the oscillatory part of 186 the DW velocity is proportional to $1/R$ and thus the area, 187 covered by its radius vector, is independent from *R* for the ¹⁸⁸ same time intervals.

To explore this finding, we define the *z* component of the ¹⁹⁰ DW "angular momentum" as $L_z = \mu R v$, where μ is the DW 191 effective mass. Assuming that the DW behaves as a parti- ¹⁹² clelike structure, we can study its dynamical properties from ¹⁹³ Newton's second law. Therefore, we define

$$
\Gamma_z = \frac{dL_z}{dt} = \mu R \frac{dv}{dt}.
$$
\n(10)

The combination of Eqs. (2) and (7) allows us to define the 195 DW effective mass μ as 196

$$
\mu = \frac{\Gamma_z}{Ra_{\theta}(t)} = \frac{M_s^2(1+\alpha^2)}{4A\gamma^2},
$$
\n(11)

where the linear acceleration is $a_{\theta}(t) = \frac{dv(t)}{dt} = \frac{dv}{d\phi}$ $\frac{d\phi}{dt}$. Thus, 197 the *z* component of the angular momentum reads

$$
L_z = \mu R v = \frac{\alpha \delta M_s^2 R H}{4\gamma A} - \frac{M_s}{\gamma} \cos \phi.
$$
 (12)

The first term results from the Zeeman interaction and reflects a small constant drift of the DW along the nanowire. The 200 second term is oscillating and it is produced by the curvatureinduced exchange-driven effective field. Note that due to the 202 time dependence of the domain wall phase $\phi(t)$, the angular 203

FIG. 3. (a) Time dependence of the DW velocity. Symbols and solid lines represent numerical and analytical results, respectively. The different colors stand for different NW curvatures: $\kappa_3 = 2.094$ (brown), $\kappa_6 = 1.047$ (blue), and $\kappa_{10} = 0.628$ (red) (10^6 m^{-1}) . Dashed lines and labels V_{AMP} highlight the amplitude of the velocity. (b) Amplitude of the velocity vs curvature. Red circles and blue line represent numerical and analytical results, respectively. Orange line is a linear fit of the numerical results. (c) Time evolution of the area covered by the DW during its dynamics. Symbols and solid lines represent numerical and analytical results, respectively. The small linear displacement of the DW along the NW has been subtracted in our numerical results.

²⁰⁴ momentum is not conserved. However, it is a conserved quan-²⁰⁵ tity if one averages over the domain wall oscillating period.

²⁰⁶ Since we are interested in the dynamical component and ²⁰⁷ the constant drift term in the velocity is relatively small, we ²⁰⁸ only focus on the oscillatory behavior, defining the quantity

 $\mathscr L$ as 209

$$
\mathcal{L} = L_z - \frac{\alpha \delta M_s^2 R H}{4\gamma A} = -\frac{M_s}{\gamma} \cos\left(\frac{\gamma H t}{1 + \alpha^2} + \frac{\pi}{2}\right).
$$
 (13)

Therefore, $\mathscr L$ is curvature independent. The rate of area 210 that a DW covers during its dynamics is related to the angular 211 momentum by 212

$$
\frac{d\mathscr{A}}{dt} = \frac{R^2}{2}\frac{d\theta_0}{dt} = \frac{L_z}{2\mu} \approx \frac{\mathscr{L}}{2\mu},\tag{14}
$$

where we again disregarded the constant drift term.

Thus, although both the area and angular momentum are 214 oscillating in time quantities, there is a simple relation be- ²¹⁵ tween them, very analogous to that in the system with a ²¹⁶ conserved angular momentum. This fact implies that the rate 217 of the area covered per time by the DW due to the curvature- ²¹⁸ induced exchange-driven effective interaction is independent 219 of the curvature. This result is central for our article and is ²²⁰ illustrated in Fig. $3(c)$, where analytical results are compared 221 with direct numerical simulations.

The Newtonian-like equations of motion for the DW have 223 the following form: 224

$$
\mu a_R = -\frac{4A}{(1 + \alpha^2)R^3} \cos^2 \phi
$$
 (15)

$$
\mu a_{\theta} = \frac{HM_s}{(1+\alpha^2)R} \sin \phi.
$$
 (16)

Equations (15) and (16) represent the centripetal-like force $_{225}$ $(-\mu v^2/R)$ and the tangential one ($\mu dv/dt$), respectively. The 226 former comes from the exchange interaction, while the latter 227 is due to the external magnetic field. These results suggest 228 some analogy to systems moving in central potential, albeit 229 in our case, the radial part of the potential has dependence 230 $1/R²$ and is oscillating in time. However, although the exchange interaction yields a central-like periodic field, one 232 should remark that the potential is not centrosymmetric due 233 to the nontrivial behavior of its tangential part. Low damping 234 values ($\alpha \ll 1$) are required for the validity of the different 235 approximations used. For this range of values, α does not play 236 any important role in the system. Additionally, the value of the 237 external magnetic field affects just the tangential acceleration 238 amplitude, which increases linearly with H .

It is important to remark that the area covered at any time, ²⁴⁰ as well as the maximum area evaluated at the semiperiod of ²⁴¹ oscillations, depends on the magnetic field strength ²⁴²

$$
\mathscr{A}(t) = \frac{2A}{HM_s} \left[1 - \cos\left(\frac{\gamma H t}{1 + \alpha^2}\right) \right],\tag{17}
$$

which is illustrated in Fig. $3(c)$. Nevertheless, the average in 243 time area covered in a half-period $(\tau/2)$, i.e., $\langle \mathcal{A} \rangle = \frac{2\mathcal{A}}{\tau} =$ 244 4*A*γ $\frac{4AY}{\pi M_s}$, is independent of the field strength. Clearly, it is also curvature independent. Furthermore, the value of $\langle \mathscr{A} \rangle$ matches 246 with the amplitude value of the oscillations for the velocity 247 (V_{AMP}) in Eq. [\(7\)](#page-2-0) with the exception of the factor π .

III. CONCLUSIONS ²⁴⁹

In conclusion, we have reduced the dynamical LLG equation of motion for a transverse DW in bent cylindrical ²⁵¹

 nanowires with a constant curvature to a Newton equation of a point nanoparticle in a centrosymmetric periodic field, pro- duced by the exchange interaction. From the analysis of the DW angular momentum along the *z* axis direction, one can observe that the term corresponding to exchange interaction is curvature independent. This result allows us to obtain the area swept by the DW in relation to the center of the NW curvature. We have observed that the area covered by the DW due to the exchange-driven effective field is the same, independent of the NW curvature. This finding is associated with the increase in the DW velocity, under the Walker regime, as a function of the NW curvature. We highlight that although the swept area is independent of the NW curvature, it is oscillating in time

 with a constant period. The results discussed in this work could be confused with Kepler's law for a DW "orbiting" in a circular trajectory around the curvature center. Nevertheless, the potential of interaction between the DW and an imaginary "mass center"

270 in the system is not of the kind $V \propto 1/R$. This fact, in addition

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to the periodicity in the DW velocity when it displaces under $_{271}$ the Walker regime, explain why, if we consider a constant 272 orbit, the DW seeps different areas in the same time interval. 273 At the same time, our results highlight that a plethora of 274 different analogies can exist in nature, providing a rich phe- ²⁷⁵ nomenological description of otherwise complicated physical 276 phenomena. 277

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