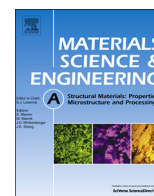




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Short communication

Phase transformation and shape memory effect of a Cu-Al-Ni-Mn-Nb high temperature shape memory alloy

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ABSTRACT

The microstructure, phase transformation and shape memory effect of the high temperature shape memory alloy Cu-11.4Al-3.2Ni-3Mn-0.5 Nb (wt%) were investigated for the first time. The shape recovery ratio can achieve 73% when submitted to 690 MPa and the compressive stress of fracture of the alloy is 1560 MPa.

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1. Introduction

High temperature shape memory alloys (HTSMAs) have been attracting the attention of research groups due to their possible suitability for engineering applications in thermosensitive devices that operate above 100 °C [1]. For this purpose, the phase transformation involving the shape memory effect must be above this temperature. The most widely used shape memory alloy (SMA) NiTi does not fit this requirement and can be only be used up to about 80 °C [2]. Therefore, many attempts have been made on the Ni-Ti system to shift the martensitic transformation to higher temperatures by the addition of different elements, thus obtaining the ternary system Ni-Ti-X (X=Zr, Pd, Hf) [3–9]. However, these alloys' drawback is their high production challenges such as high reactivity of the elements with oxygen and furthermore the high production costs associated. Hence, the search for new systems with shape memory effect (SME) promoted the study of Cu-based SMA such as Cu-Zn-Al, Cu-Al-Ni, Cu-Al-Nb, Cu-Al-Ta and Cu-Al-Fe [10–16]. Despite the well-known brittleness of the polycrystalline Cu-Al-Ni SMA, it still attracts the attention of researchers because it is one system that fits all the requirements of a HTSMA. Many attempts to improve the mechanical properties of the Cu-Al-Ni

alloys have been achieved by the addition of elements, such as Mn, B, Ti, V, Zr, Co, [17] but also by refinement of the microstructure by different thermomechanical processing routes [18–23]. Nonetheless there are still many application problems that require further work on these systems. To design a good HTSMA that can be used at high temperature without degrading its properties several aspects such as the mechanical properties, the thermal stability (usually around 100–200 °C for Cu-based alloys) and an acceptable recoverable transformation strain level (> 0.5%) [24] combined with a high recovery stress (> 200 MPa) should be considered [1,17]. Therefore, this work investigates the shape memory effects and the phase transformation of a Cu-Al-Ni-Mn alloy with a small addition of Nb produced by spray-forming. Preliminary results on this HTSMA show an extraordinary behavior: the maximum recovery strain achieved was around 1% when subjected to 690 MPa, with a recovery ratio of 73%.

2. Materials and methods

The Cu-11.35Al-3.2Ni-3Mn-0.5Nb (wt%) alloy was prepared by spray-forming. Details of the process can be found at [19]. The composition measured by Inductively Coupled Plasma-Atomic Emission Spectrometry (ICP-OES) was Cu-11.29Al-3.10Ni-2.85Mn-0.35Nb (wt%). The microstructure was analyzed by optical microscopy, scanning electron microscopy (SEM, Philips XL 30 FEG-SEM), X-ray diffraction with Cu K α radiation (XRD, Siemens

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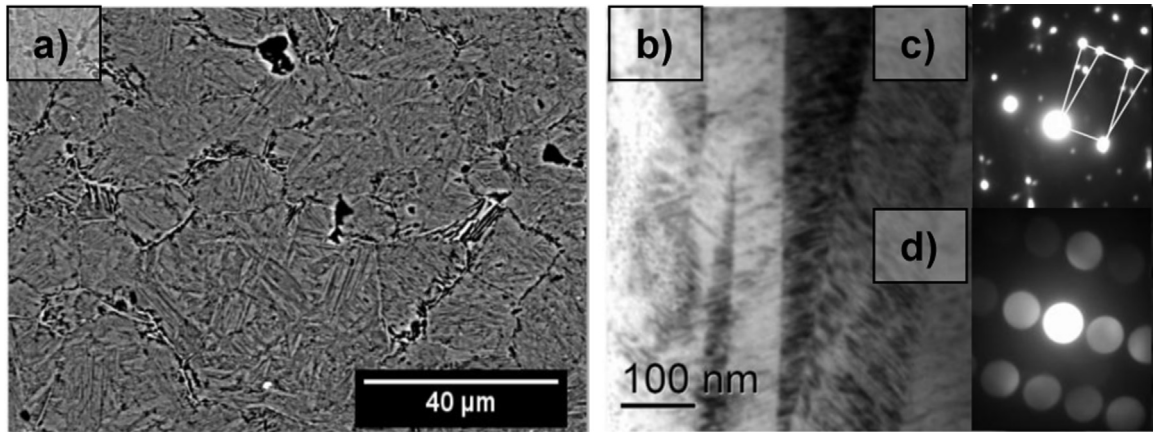


Fig. 1. (a) SEM micrograph of the as-deposited alloy. (b) Bright field TEM image showing the martensite twinned laths, (c) SAED near the [100] zone axes from several martensite variants and (d) convergent beam diffraction from one of the martensite variants along [100] zone axes of the β' monoclinic martensite.

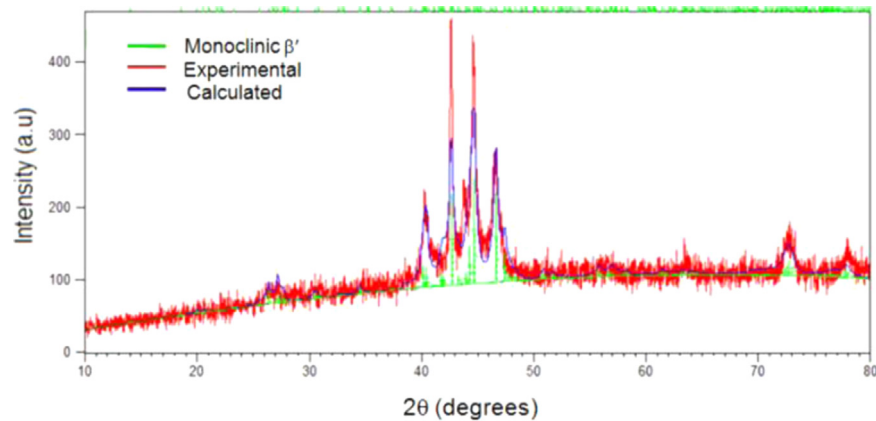


Fig. 2. XRD pattern of the deposited alloy.

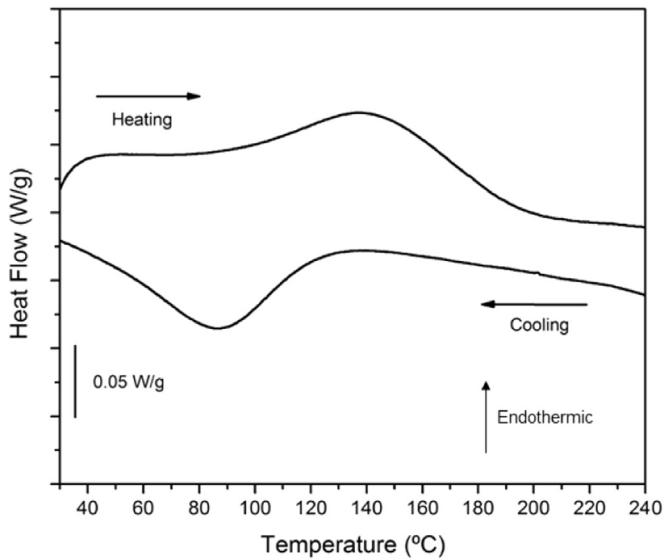


Fig. 3. DSC curves of the studied alloy.

Table 1
Transformation temperatures A_s , A_f , M_s , A_f-A_s , A_f-M_s ($^{\circ}\text{C}$) and the melting point T_m for the alloy. The deviation is ± 1 $^{\circ}\text{C}$.

A_s	A_f	A_p	M_s	A_f-A_s	A_f-M_s	T_m
94	195	138	125	101	71	1003

D5005) and transmission electron microscope (TEM, JEOL 2000FX, at 200 kV). Differential scanning calorimetry (DSC, NETZSCH 200 F3 calorimeter) was carried out at a rate of 40 $^{\circ}\text{C}/\text{min}$ in order to measure the temperatures of the martensitic/austenitic phase transformation. The compression tests were performed on a Testometric Micro 500–50 kN with crosshead speed of 0.5 mm/min, using cylindrical specimens with 4 mm in diameter and 8 in length. The SME was evaluated with different pre-stress applied on the samples and analyzed based on the original sample length (l_0), length after unloading (l_1) and length after heat treatment (l_2). The heat treatment was done above the final austenitic temperature (A_f) at 280 $^{\circ}\text{C}$ for 10 min. The residual strain after unloading (ϵ_r) and the recovery strain (ϵ_{SME}) were calculated as: $\epsilon_r = (l_0 - l_1)/l_0 \times 100\%$, and $\epsilon_{\text{SME}} = (l_2 - l_1)/l_0 \times 100\%$, respectively. The recovery ratio was calculated as: $R = (\epsilon_{\text{SME}}/\epsilon_r)$.

3. Results and discussion

Fig. 1(a) shows the microstructure at room temperature of the as-deposited alloy. The microstructure is homogeneous and no heat treatments were performed after the processing of the alloy. The austenitic originated grain size and the porosity are 24.1 ± 1.4 μm and $0.5 \pm 0.3\%$, calculated using a method showed in [25]. The grain size was refined around 82% when compared with others alloys with similar composition but without Nb content, and similar processing route, for which the grain size is around 135 μm [26]. Twinned martensitic laths can be observed inside the grains originated in the austenitic field. These laths correspond to

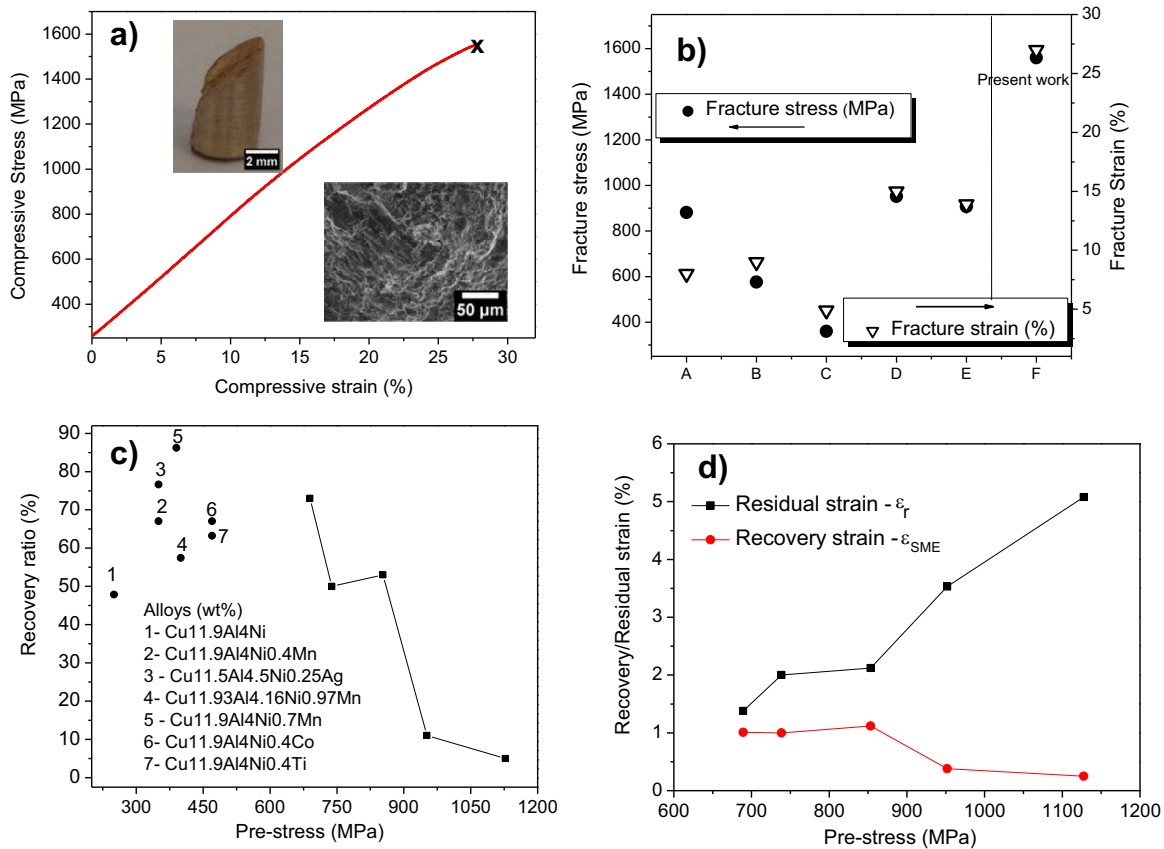


Fig. 4. (a) Compressive stress–strain curve for the Cu-11.35Al-3.2Ni-3Mn-0.5Nb (wt%) alloy. The inset figures correspond to the fractured specimen. Figure (b) corresponds to values of the fracture stress and strain for other alloys in the literature, where A=Cu11.92Al3.78Ni (homogenized at 950 °C for 120 min), B=Cu11.92Al3.78Ni (homogenized at 950 °C for 40 min), C=Cu11.92Al3.78Ni (homogenized at 650 °C for 40 min) [36], D=CuAl11.6Ni3.9Mn2.5 [37], E=Cu11.85Al3.2Ni3.0Mn [not published], all in wt%. Figure (c) shows the recovery ratio for the present alloy and alloys in the literature: 1 [36], 2 [38], 3 [39], 4 [38], 5 [38], 6 [40] and 7 [41]. Figure (d) shows the recovery strain after heat treatment above A_f and residual stress after the pre-load.

Table 2
Lattice parameters and transformation stretches for the present studied alloy and Cu-Al-Ni-Mn alloys in the literature.

Composition (wt%)		Cu11.35Al3.2Ni3Mn0.5Nb	Cu11.9Al4Ni	Cu11.9Al4Ni0.4Mn	Cu11.9Al4Ni0.7Mn	Cu11.9Al4Ni1.0Mn
Lattice parameters (nm)	a	0.4500	0.4425	0.4428	0.4421	0.4428
	b	0.5224	0.525	0.5272	0.5256	0.5252
	c	1.2825	3.8055	3.8046	3.7925	3.8043
	θ	95.6°	89.9°	90.4°	90.3°	90.1°
Transformation stretches	α	0.7730	0.7601	0.7606	0.7594	0.7606
	β	0.6345	0.6377	0.6404	0.6384	0.6379
	γ	1.5578	4.6223	4.6212	4.6065	4.6208
Eigenvalue λ_2	-	0.76811	0.76010	0.76060	0.75940	0.76061
det(U)	-	0.7640	2.2404	2.2508	2.2333	2.2421
Reference	-	Present study	[41]	[39]	[39]	[39]

different variants of martensites. TEM bright field image from the as-cast samples shows nanoscale twinned martensites can be seen in Fig. 1(b). The selected area electron diffraction (SAED) from this region along the [100] zones axis of the martensites is shown in Fig. 2(c). The diffracted spots show reflections from different martensites variants. Its indexation gives interplanar distances corresponding to the monoclinic β' phase. The convergent beam electron diffraction in Fig. 1(c) was taken from one variant and shows the reflections from the [100] zone axis and corroborates the previous SAED. Fig. 2 shows the XRD diffraction pattern of the alloy at room temperature. One predominant phase, the monoclinic β' , was found, corroborating what was observed by TEM. The indexation of the cell parameters using the Rietveld method gave the lattice parameters shown in Table 2.

Fig. 3 shows the DSC curve for the Cu-11.35Al-3.2Ni-3Mn-0.5Nb

(wt%). An endothermic peak on the heating step characterizes the reverse transformation, whereas the forward transformation shows an exothermic on the cooling step. The transformation temperature was taken from the second DSC cycle in order to eliminate the influence of any quenched-in vacancies. Table 1 presents the transformation temperatures A_s , A_f , M_s , $A_f - A_s$, $A_f - M_s$ (°C) and the melting point T_m for the as-deposited sample. It can be observed that the onset austenitic start (A_s) and final (A_f) transformation temperatures are 94 °C and 195 °C, respectively. It is worth noticing that the transformation temperatures are generally affected by the grain sizes; the larger the grain sizes the higher the transformation temperatures [10]. However, for this new alloy composition the grain size has been refined and the transformation temperature remains high. This fact contributes for a HTSMA with better mechanical properties. The interval ($A_f - A_s$)

is related to the elastic energy accumulated in the accommodation of the martensitic variants [27,28], therefore it can be said that the narrower its value, the easier it is for the martensites to accommodate within the austenite in this range of temperature. Thus, this interval is so called the elastic hysteresis. For the present alloy this value is around 101 °C and can be considered as a broad hysteresis. The elastic energy stored is calculated by the expression $E_{el} = \Delta S (A_f - A_s)$ [27,28] which is 3.79 J/g. The frictional dissipated energy, which can be related to the damping properties of the material, is related with the interval $(A_f - M_s)$ that is around 71 °C. The dissipated energy is calculated from the following expression $E_d = \Delta S(A_f - M_s)/2$ [27,28], and is equal to 1.32 J/g. The values of E_{el} and E_d for similar composition without Nb and processed by the same route were 0.55 J/g and 0.29 J/g [19] respectively. Therefore, the use of Nb in the alloy makes the nucleation of the martensite more difficult, forcing the elastic energy and frictional energy to increase. This fact can be explained by the refined variants of martensite (around 100 nm), as seen in Fig. 1(b), that makes higher the interface boundaries between the variants. It disadvantages the elastic accommodation of the variants and disturb the movement of the interfaces, making the frictional energy to increase [29]. The refined laths as well as the refined grains affect the mechanical properties, as will be further discussed.

Fig. 4(a) shows the compressive stress–strain behavior of the alloy at room temperature. The compressive fracture stress and strain were 1560 MPa and 27%, respectively. The main mechanism of deformation for this alloy is the reorientation and detwinning of the martensite variants, as found in many SMA, i.e. NiTi and Cu–Al–Ni [26,30,31]. As shown by XRD the predominant phase is the monoclinic β' martensite. Thus, the influence of other possible phases in small volume fraction is considered negligible in the mechanical behavior of the alloy. The refined grain and refined martensite laths in the microstructure might be the responsible for its high fracture stress. As the mechanism of deformation involves the movement of the martensites variants, the deformation will be more difficult when the size of the variants is small because of the greater number of interfaces. It will require more energy to move them and therefore higher values of stresses. For the present alloy, the value of the hysteresis $|A_f - M_s|$ reflects there is a larger frictional energy between the variants. As shown before $|A_f - M_s| = 71$ °C, which is considered a broad hysteresis if compared with other Cu–Al–Ni-based alloys. Fig. 4(b) compares the fracture stress and fracture strain in compression mode for other Cu–Al–Ni and Cu–Al–Ni–Mn alloys with similar composition with the alloy in the present study. It can be seen that the Cu–11.35Al–3.2Ni–3Mn–0.5Nb (wt%) studied in this work presents considerably higher values than all the others alloys (65% higher than the best of the other alloys; alloy D).

The shape recovery ratio can be seen on Fig. 4(c). It retains a value of more than 40% of recovery when the sample is subject to 900 MPa and an outstanding shape recovery ratio of 73% when subject to 690 MPa, which has never been reported for Cu–Al–Ni-based high temperature alloy for this value of stress. For greater stresses, the shape recovery ratio decreases to less than 10% for stresses higher than 950 MPa. When compared to other HTSMA reported in the literature as shown in Fig. 4(c), it can be observed that the same value of the recovery ratio happens at lower stresses. In this case, it can be calculated that the recovery ratio is better for the studied alloy because of the absence or at least a less pronounced plastic deformation mechanism with the imposed pre-stresses values. The recent developed theory using the geometric compatibilities and crystalline symmetry between the austenite and martensite, the so-called geometric non-linear theory of martensite (GNLTM) [32] can explain the superior behavior of this alloy in comparison to others. This theory states that a small volume change and a crystalline compatibility between the

austenite and martensite are two important factors for the thermoelasticity of the transformation [33–36]. Using the lattice parameters of the austenite and the martensite and the transformation stretches α , β and γ it is possible to obtain the deformation matrix for the cubic to monoclinic phase transformation using the following relationships $\alpha = a/a_0$, $\beta = b/(a_0\sqrt{2})$, $\gamma = c/(a_0\sqrt{2})$, where a_0 is the lattice parameter of the cubic unit cell and a , b and c are the lattice parameters of the monoclinic unit cell [34,35]. Eq. (1) shows the deformation matrix for one variant of the monoclinic martensite for the studied alloy. From the deformation matrix it is possible to measure the compatibility of the austenite and the martensite and the volume change in the phase transformation. The middle eigenvalue λ_2 is the parameter that measures the misfit between the austenite and martensite and when it is equal to 1 it means that the austenite is directly compatible with the martensite. The volume change is measured by $\det(U)$ and when it is equal to 1 means that there is no volume change due to the transformation [32–35]. Table 2 shows λ_2 and $\det(U)$ for the Cu–11.35Al–3.2Ni–3Mn–0.5Nb (wt%) alloy and others Cu–Al–Ni–Mn of the literature with similar composition. It can be seen that for the present alloy both parameters are closer to one than the others. This explains the enhanced shape memory recovery of this alloy. Details of the calculation can be found in [35].

$$U = \begin{pmatrix} 0.7713 & -0.0357 & -0.0357 \\ 0.0357 & 1.0957 & 0.4612 \\ -0.0357 & 0.4612 & 1.0957 \end{pmatrix} \quad (1)$$

The recovery strain on Fig. 4(d) remains being 1% up to 900 MPa and then decreases in the same interval as the shape recovery ratio, which means that some mechanism of plastic deformation is acting around these values of stress, hindering the reversible martensitic transformation to the original twinned orientation of the variants, which affects the shape memory effect [37]. This fact is confirmed by the residual stress increasing after 900 MPa, as seen in Fig. 4(d).

4. Conclusion

In summary, the phase transformation and shape memory properties of the Cu–Al–Ni–Mn with a minor addition of Nb produced by spray forming have been investigated for the first time. It was found that Cu–11.35Al–3.2Ni–3Mn–0.5Nb (wt%) presented shape recovery ratio of 73% when subject to 690 MPa of compressive stress. The fracture stress for the alloy was around 1560 MPa. This new, Cu–11.35Al–3.2Ni–3Mn–0.5Nb (wt%) alloy has proven to be a good candidate for applications at high temperature (> 200 °C, when $T > A_f$), where a shape memory phase transformation can be used, such as in actuation and damping devices.

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