



## Data Article

# Density, viscosity, excess molar volume and viscosity deviation for [chloroform (1) + di-isopropyl-ether(2) + 1-propanol (3)] ternary system at 298.15 K.



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## ABSTRACT

Densities  $\rho$  and viscosity  $\eta$  of the [chloroform (1)+di-isopropyl ether (DIPE) (2)+ 1-propanol (3)] ternary system have been measured at 298.15 K and pressure of 960 hPa using an Anton Paar DMA 500 stavgimeter. Excess molar volumes  $V^E$  and viscosity deviation  $\Delta\eta$  were calculated. The excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for binary and ternary systems were correlated by a Redlich-Kister and Nagata and Tamura type equation. Also, the ternary excess molar volume and viscosity deviation  $Y_{123}^E$  were predicted using the Radojković equation. From the macroscopic behavior inferences were made about the molecular interactions in the ternary mixture.

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Subject area	Physical chemistry
Compounds	Chloroform; di-isopropyl ether (DIPE); 1-propanol
Data category	Physicochemical
Data acquisition format	Physical properties
Data type	Raw, analyzed, and calculated
Procedure	Determination: density with vibrating tube densimeter viscosity with concentric cylinder viscometer, Hall effect
Data accessibility	Excess molar volume and viscosity deviation are calculated with the general expressions In this article

## 1. Rationale

The importance of experimental data of binary and ternary systems is well known, both from the viewpoint of chemical engineering applications and the possibility of drawing conclusions about the interactions between the components of the mixture [1–4].

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The information available in the open literature of the thermophysical properties of the binary systems studied is very scarce, particularly in the systems where DIPE is present. The ternary system presented here was not studied, according to exhaustive search carried out. Thus, these data are very useful for the scientific and technological community, mainly if the fact that both alkanols and ethers are used as fuel additives is taken into account.

In this paper we report density and viscosity data at  $T=298.15$  K and 960hPa of three pure chemicals (chloroform, DIPE and 1-propanol), as well as for the [chloroform (1)+1-propanol (3)] binary system and the [chloroform (1)+DIPE (2)+1-propanol(3)] ternary liquid mixture over the whole composition range. Empiric equations for the excess molar volumes  $V^E$  and viscosity deviation  $\Delta\eta$  of the binary system as well as for the ternary system as a function of composition were developed using Origin Pro 8.5. These equations were fitted using least squares with all points equally weighted. The appropriate number of constants and significant digits are obtained by comparing with the experimental errors.

The binary systems [chloroform (1)+DIPE (2)] and [DIPE (2)+1-propanol (3)], were already studied and published by our research group [5,6].

The excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for binary system were fitted to a Redlich-Kister [7] type equation. The ternary excess molar volumes  $V^E$  and viscosity deviation  $\Delta\eta$  were correlated by a Redlich-Kister [7] type equation and Nagata and Tamura [8] type equation using least squares in order to obtain their respective dependency on concentration. The parameters calculated with the Redlich-Kister equation [7] for the binary systems [DIPE (2)+1-propanol (3)] and [chloroform (1)+1-propanol (3)], reported in previous works [5,6], were used in the terms for the binary contribution of Nagata and Tamura [8] type equation. Also, the ternary excess molar volume and viscosity deviation  $Y_{123}^E$  were predicted using the Radojković [9] equation. In all cases Origin Pro 8.5 was used.

We found papers on density [10] and two on viscosity [10,11] data of the binary system [chloroform (1)+1-propanol ((3)) and experimental values of these reagents. To our knowledge no data density and viscosity, or excess molar volume values and viscosity deviation of [chloroform (1)+di-isopropyl ether (DIPE) (2)+1-propanol (3)] ternary system have been published.

## 2. Procedure

### 2.1. Reagents

Chloroform (p.a.) and 1-propanol (p.a.) were supplied by Dorwill, while DIPE (p.a.) was supplied by MERK (Germany). The purity of the reagents used was controlled by chromatography and IR spectroscopy which guarantees its purity, and the instruments used are certified by the manufacturer and monitored regularly, each time a series of measurements starts. The purity of the reagents, determined by gas chromatography was 99.8%.

### 2.2. Measurements

Liquid mixtures were prepared by mass in airtight-stoppered bottles. The same techniques described in previous publication [12] were used for the preparation of samples. The same instruments described in previous publications [13] were used. Density and viscosity were simultaneously measured with an Anton Paar Stabinger viscometer (SVM 30 0 0/G2). Total uncertainties in this work are  $\pm 0.0001$  mPa.s for viscosity value,  $\pm 0.1$  kg/m<sup>3</sup> for density, and  $\pm 0.01$  K for temperature. The uncertainty in the mole fractions for these mixtures is estimated to be around  $\pm 1 \times 10^{-4}$ .

Ternary mixtures were prepared from binary mixtures of constant molar fraction ratio  $\gamma_k = x_{1k}/x_{2k}$  and adding known volumes of the third component. Each set of ternary mixtures with a constant molar fraction ratio  $\gamma_k = x_{1k}/x_{2k}$  is called series and k the number of serie. In this case, the starting binary system was [chloroform (1)+DIPE (2)].

At least three measurements were made for each solution or pure component.

### 2.3. Excess molar volumes and viscosity deviation

The excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for the binary and ternary systems were calculated from the following equations:

$$V^E = \sum_{i=1}^n x_i M_i \left[ \left( \frac{1}{\rho} \right) - \left( \frac{1}{\rho_i} \right) \right] \quad (1)$$

$$\Delta\eta = \eta - \left( \sum_{i=1}^n \eta_i x_i \right) \quad (2)$$

Where n is the number of components,  $x_i$  the mole fraction of component i in the mixture,  $M_i$  its molecular weight,  $\rho$ ,  $\eta$ , are the density and viscosity of the mixture and  $\eta_i$ ,  $\rho_i$  are the measured densities and viscosities of the pure component, respectively.

Excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  of the binary systems were fitted using the Redlich-Kister [7] polynomial equation of the type:

$$Y_{ij} = x_i x_j \sum_{p=0}^k a_p (1 - 2x_i)^p \quad (3)$$

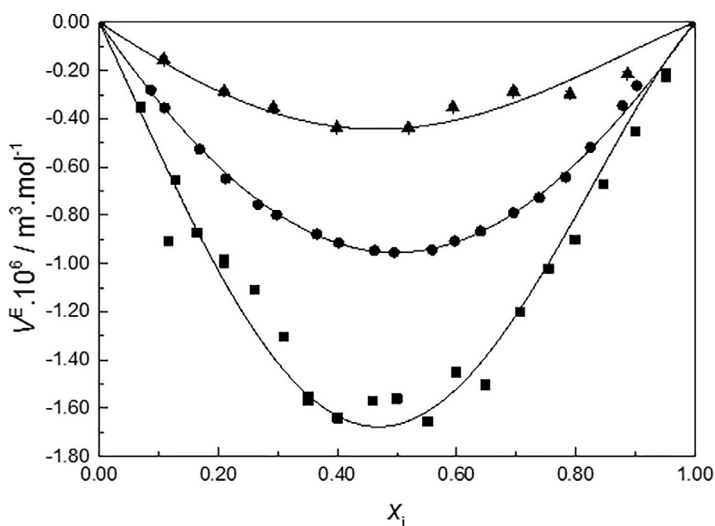


Fig. 1. Experimental values of  $V^E$  against  $x_i$  ( $i=1,2$ ) for binary systems:(■): [chloroform (1)+ dipe (2)]; (●):[chloroform (1)+ 1-propanol (3)] and (▲) :[dipe (2)+ 1-propanol (3)] at  $(298.15 \pm 0.01)$  K.

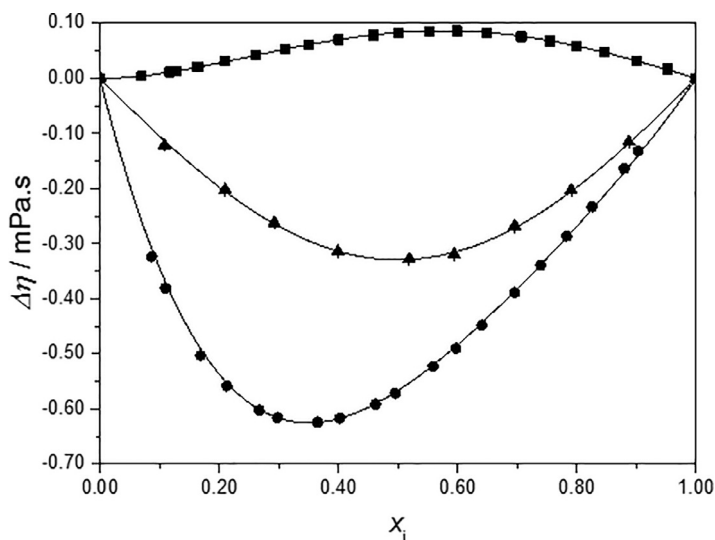


Fig. 2. Experimental values of  $\Delta\eta$  against  $x_i$  ( $i=1,2$ ) for binary systems:(■): chloroform (1)+ dipe (2); (●): [chloroform (1)+ 1-propanol (3)] and (▲) :[dipe (2)+ 1-propanol (3)] at  $(298.15 \pm 0.01)$  K.

$Y_{ij}$  is the excess property of the  $ij$  binary system and  $a_p$  are adjustable parameters. These equations were fitted using least squares [14] with all points equally weighed. The appropriate number of constants and significant digits are obtained by comparison with the experimental errors mentioned above.

A series of equations was proposed that adjust the excess properties and the deviations of the ideality of the ternary systems. Some of these equations adjust the excess properties from those of the binary systems [15–17]. There are several articles in the literature [17–20] that use these proposals. Also in some ternary systems the applicability of associated solution models was evaluated [21].

In this paper, the ternary excess molar volumes and viscosity deviation  $Y_{123}^E$  were predicted using the Radjković equation [9]:

$$Y_{123}^E = Y_{12}^E + Y_{13}^E + Y_{23}^E \quad (4)$$

Where  $Y_{12}^E$ ,  $Y_{13}^E$ ,  $Y_{23}^E$  are the excess molar volume or viscosity deviation for the three binary systems.

Also, the ternary excess molar volumes  $V^E$  and viscosity deviation  $\Delta\eta$  were correlated by Nagata and Tamura equation type [8]:

$$Y_{123}^E = Y_{12}^E + Y_{13}^E + Y_{23}^E + x_1x_2x_3 \times R \times T \times (B_0 - B_1x_1 - B_2x_3 - B_3x_1^2 - B_4x_2^2 - B_5x_1x_2 - B_6x_1^3 - B_7x_2^3 - B_8x_1^2x_2) \quad (5)$$

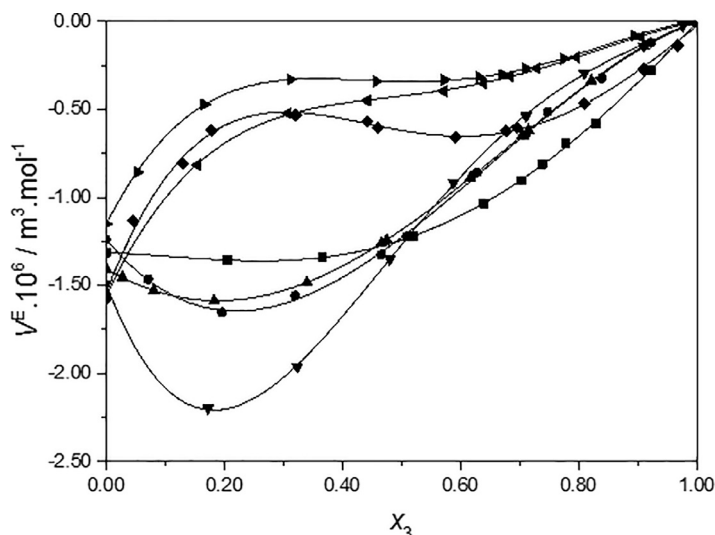


Fig. 3. Experimental values of  $V^E$  against  $X_3$  for series ■ :  $S_1$  , ● :  $S_2$  , ▲ :  $S_3$  , ▼ :  $S_4$  , ◆ :  $S_5$  , ◀ :  $S_6$  and ▶ :  $S_7$  at  $(298.15 \pm 0.01)$  K.

Table 1

Densities and viscosities of the pure components at  $(298.15 \pm 0.01)$  K.

Reagent	$\rho$ / $\text{kg}\cdot\text{m}^{-3}$		$\eta$ / $\text{mPa}\cdot\text{s}$	
	Experimental	Literature	Experimental	Literature
Chloroform	1478.4	1478.82 [11]	0.5357	0.556 [11]
		1479.70 [22]		0.5357 [22]
		1478.8 [13]		0.556 [13]
Dipe	718.2	718.54 [22]	0.3791	0.379 [22]
1-propanol	799.8	786.30 [11]	1.8343	1.8468 [11]
		799.60 [23]		1.9430 [23]

Experimental uncertainties u:  $u(T)=0.01$  K,  $u(\rho)=0.1$   $\text{kg}\cdot\text{m}^{-3}$ ,  $u(\eta)=0.0001$   $\text{mPa}\cdot\text{s}$ .

and the Redlich-Kister equation type [7]:

$$Y_{123}^E = Y_{12}^E + Y_{13}^E + Y_{23}^E + x_1 x_2 x_3 \cdot [B_0 + B_1 \cdot (x_1 - x_2) + B_2 \cdot (x_2 - x_3) + B_3 \cdot (x_1 - x_3) + B_4 \cdot (x_1 - x_2)^2 + B_5 \cdot (x_2 - x_3)^2 + B_6 \cdot (x_1 - x_3)^2 + \dots] \quad (6)$$

Where  $B_n$  are the adjustable parameters obtained from fitting the  $V^E$  and  $\Delta\eta$  data (calculated from experimental data). In this work a modified version of the Nagata –Tamura equation is proposed.

$$Y_{123}^E = x_1 x_2 x_3 \times R \times T \times (B_0 - B_1 x_1 - B_2 x_3 - B_3 x_1^2 - B_4 x_2^2 - B_5 x_1 x_2 - B_6 x_1^3 - B_7 x_2^3 - B_8 x_1^2 x_2) \quad (7)$$

In all cases we calculate the standard deviations using the equation:

$$\sigma = \sqrt{\left( \frac{\sum_{i=1}^N (Y_{\text{exp}}^E - Y_{\text{calc}}^E)^2}{N - p} \right)} \quad (8)$$

Figs. 1 and 2 show excess molar volume and viscosity deviation plotted against the mole fraction of chloroform for the systems: [chloroform (1)+DIPE (2)] and [chloroform (1)+1-propanol (3)] and against the mole fraction of DIPE for the system [DIPE (2)+1-propanol (3)] at 298.15 K.

Figs. 3 and 4 show the behavior of the excess molar volume and viscosity deviation plotted against the mole fraction of 1-propanol (3) for the different series studied in this work at 298.15 K.

Figs. 5 and 6 show surface of the excess molar volume and viscosity deviation against molar fractions of DIPE (2) and 1-propanol (3).

Figs. 7 and 8 show contour lines of excess molar volume and viscosity deviation for the [chloroform (1)+DIPE(2)+1-propanol(3)] at 298.15 K, respectively.

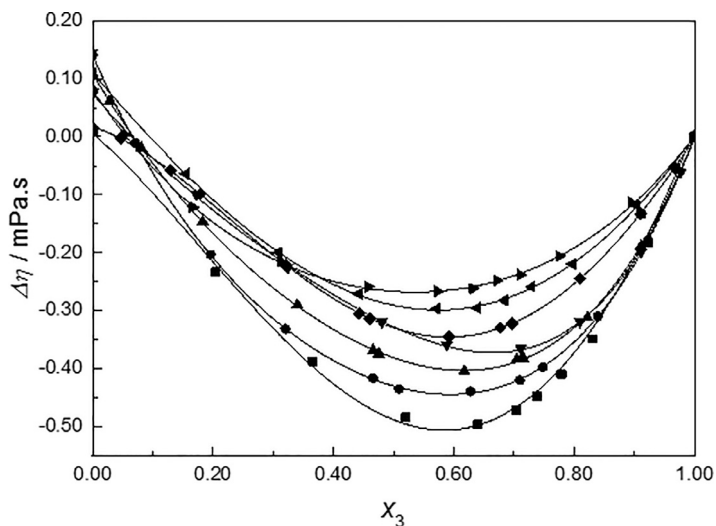
Origin Pro 8.5 was used for all the figures.

**Table 2**

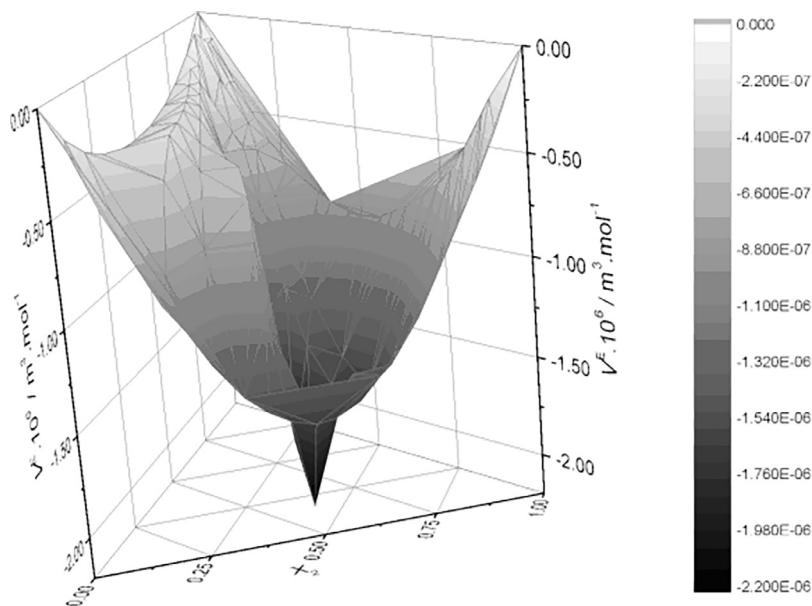
Experimental density  $\rho$  and viscosity  $\eta$  for the [chloroform (1)+1-propanol (3)] binary system at  $(298.15 \pm 0.01)$  K.

$x_1$	$\rho / \text{kg/m}^3$	$\eta / \text{mPa}\cdot\text{s}$	$V^E / \text{m}^3/\text{mol}$	$\Delta\eta / \text{mPa}\cdot\text{s}$
Chloroform (1)+1-propanol (3)				
0.0000	800.0	1.9732	0.00	0.00
0.1081	883.1	1.6982	$-1.63 \cdot 10^{-7}$	-0.095
0.2102	955.0	1.4729	$-2.86 \cdot 10^{-7}$	-0.179
0.2919	1010.0	1.2968	$-3.54 \cdot 10^{-7}$	-0.241
0.3989	1089.9	1.0941	$-3.92 \cdot 10^{-7}$	-0.297
0.5188	1170.1	0.9102	$-4.11 \cdot 10^{-7}$	-0.314
0.5941	1220.1	0.8129	$-3.84 \cdot 10^{-7}$	-0.308
0.6958	1279.9	0.7201	$-3.35 \cdot 10^{-7}$	-0.259
0.7900	1340.0	0.6508	$-2.67 \cdot 10^{-7}$	-0.197
0.8869	1403.2	0.6019	$-1.84 \cdot 10^{-7}$	-0.112
1.0000	1470.2	0.5580	0.00	0.000

Experimental uncertainties  $u$ :  $u(T) = 0.01$  K,  $u(\rho) = 0.1 \text{ kg}\cdot\text{m}^{-3}$ ,  $u(\eta) = 0.0001 \text{ mPa}\cdot\text{s}$



**Fig. 4.** Experimental values of  $\Delta\eta$  against  $X_3$  for series  $\blacksquare$ :  $S_1$ ,  $\bullet$ :  $S_2$ ,  $\blacktriangle$ :  $S_3$ ,  $\blacktriangledown$ :  $S_4$ ,  $\blacklozenge$ :  $S_5$ ,  $\blacktriangleleft$ :  $S_6$  and  $\blacktriangleright$ :  $S_7$  at  $(298.15 \pm 0.01)$  K.



**Fig. 5.** 3D surface of excess molar volume  $V^E$  against molar fractions of chloroform ( $x_1$ ) and dipe( $x_2$ )+1-propanol ( $x_3$ ) at  $(298.15 \pm 0.01)$  K.

**Table 3**

Experimental density  $\rho$  and viscosity  $\eta$ , excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for the [chloroform (1)+DIPE (2)+1-propanol ((3))] ternary system at (298.15  $\pm$  0.01) K.

$X_1$	$X_3$	$\rho$ / kg/m <sup>3</sup>	$\eta$ / mPa.s	$V^E$ m <sup>3</sup> /mol	$\Delta\eta$ / mPa.s
$\delta_1 = 0.28910$					
0.1984	0.0000	820.1	0.4183	-1.31.10 <sup>-6</sup>	8.21.10 <sup>-3</sup>
0.1577	0.2050	819.6	0.4689	-1.35.10 <sup>-6</sup>	-2.33.10 <sup>-1</sup>
0.1257	0.3664	818.8	0.5440	-1.34.10 <sup>-6</sup>	-3.88.10 <sup>-1</sup>
0.0952	0.5203	817.0	0.6666	-1.22.10 <sup>-6</sup>	-4.84.10 <sup>-1</sup>
0.0714	0.6400	814.6	0.8251	-1.03.10 <sup>-6</sup>	-4.96.10 <sup>-1</sup>
0.0587	0.7039	812.9	0.9410	-9.04.10 <sup>-7</sup>	-4.71.10 <sup>-1</sup>
0.0518	0.7389	811.7	1.0150	-8.09.10 <sup>-7</sup>	-4.47.10 <sup>-1</sup>
0.0439	0.7788	810.2	1.1098	-6.94.10 <sup>-7</sup>	-4.09.10 <sup>-1</sup>
0.0338	0.8294	808.5	1.2424	-5.80.10 <sup>-7</sup>	-3.49.10 <sup>-1</sup>
0.0153	0.9231	804.1	1.5410	-2.75.10 <sup>-7</sup>	-1.83.10 <sup>-1</sup>
0.0000	1.0000	799.8	1.8340	0.00	0.00
$\delta_2 = 0.49047$					
0.2957	0.0000	873.2	0.5660	-1.24.10 <sup>-6</sup>	1.41.10 <sup>-1</sup>
0.2746	0.0713	872.2	0.515	-1.46.10 <sup>-6</sup>	-1.08.10 <sup>-2</sup>
0.2377	0.1959	868.7	0.4981	-1.65.10 <sup>-6</sup>	-2.03.10 <sup>-1</sup>
0.2009	0.3206	862.5	0.545	-1.56.10 <sup>-6</sup>	-3.32.10 <sup>-1</sup>
0.1580	0.4657	853.3	0.665	-1.33.10 <sup>-6</sup>	-4.16.10 <sup>-1</sup>
0.1451	0.5092	850.0	0.708	-1.22.10 <sup>-6</sup>	-4.35.10 <sup>-1</sup>
0.1100	0.6279	839.5	0.870	-8.58.10 <sup>-7</sup>	-4.39.10 <sup>-1</sup>
0.0859	0.7096	831.9	1.005	-6.47.10 <sup>-7</sup>	-4.20.10 <sup>-1</sup>
0.0746	0.7478	827.8	1.082	-5.14.10 <sup>-7</sup>	-3.97.10 <sup>-1</sup>
0.0475	0.8395	818.5	1.298	-3.22.10 <sup>-7</sup>	-3.10.10 <sup>-1</sup>
0.0228	0.9227	808.9	1.547	-1.21.10 <sup>-7</sup>	-1.78.10 <sup>-1</sup>
0.0000	1.0000	799.8	1.834	0.00	0.00
$\delta_3 = 0.79141$					
0.4038	0.0000	940.6	0.552	-1.41.10 <sup>-6</sup>	1.10.10 <sup>-1</sup>
0.3927	0.0276	938.7	0.541	-1.45.10 <sup>-6</sup>	6.03.10 <sup>-2</sup>
0.3711	0.0811	934.9	0.535	-1.53.10 <sup>-6</sup>	-1.98.10 <sup>-2</sup>
0.3300	0.1829	926.5	0.550	-1.59.10 <sup>-6</sup>	-1.47.10 <sup>-1</sup>
0.2666	0.3398	910.3	0.625	-1.48.10 <sup>-6</sup>	-2.90.10 <sup>-1</sup>
0.2156	0.4662	894.4	0.723	-1.26.10 <sup>-6</sup>	-3.68.10 <sup>-1</sup>
0.2119	0.4753	893.2	0.729	-1.24.10 <sup>-6</sup>	-3.75.10 <sup>-1</sup>
0.1544	0.6176	872.0	0.898	-8.91.10 <sup>-7</sup>	-4.04.10 <sup>-1</sup>
0.1192	0.7049	857.2	1.040	-6.31.10 <sup>-7</sup>	-3.83.10 <sup>-1</sup>
0.1150	0.7152	855.5	1.056	-6.14.10 <sup>-7</sup>	-3.82.10 <sup>-1</sup>
0.0719	0.8219	836.1	1.278	-3.49.10 <sup>-7</sup>	-3.08.10 <sup>-1</sup>
0.0358	0.9113	818.3	1.522	-1.35.10 <sup>-7</sup>	-1.89.10 <sup>-1</sup>
0.0000	1.0000	799.8	1.834	0.00	0.00
$\delta_4 = 1.08051$					
0.4804	0.0000	993.0	0.528	-1.49.10 <sup>-6</sup>	7.37.10 <sup>-2</sup>
0.3974	0.1728	978.1	0.593	-2.20.10 <sup>-6</sup>	-9.97.10 <sup>-2</sup>
0.3247	0.3241	954.9	0.676	-1.96.10 <sup>-6</sup>	-2.26.10 <sup>-1</sup>
0.2497	0.4804	924.4	0.798	-1.35.10 <sup>-6</sup>	-3.20.10 <sup>-1</sup>
0.1978	0.5884	901.1	0.907	-9.14.10 <sup>-7</sup>	-3.59.10 <sup>-1</sup>
0.1387	0.7113	873.4	1.070	-5.37.10 <sup>-7</sup>	-3.65.10 <sup>-1</sup>
0.0915	0.8095	849.8	1.253	-2.92.10 <sup>-7</sup>	-3.19.10 <sup>-1</sup>
0.0428	0.9109	824.3	1.512	-1.39.10 <sup>-7</sup>	-1.99.10 <sup>-1</sup>
0.0113	0.9766	806.3	1.741	-2.32.10 <sup>-8</sup>	-6.10.10 <sup>-2</sup>
0.0000	1.0000	799.8	1.834	0.00	0.00
$\delta_5 = 1.64289$					
0.5844	0.0000	1071.5	0.4870	-1.58.10 <sup>-6</sup>	1.64.10 <sup>-2</sup>
0.5575	0.0461	1058.6	0.5310	-1.13.10 <sup>-6</sup>	-2.41.10 <sup>-3</sup>
0.5088	0.1294	1039.5	0.5890	-8.06.10 <sup>-7</sup>	-5.80.10 <sup>-2</sup>
0.4799	0.1788	1027.8	0.6160	-6.17.10 <sup>-7</sup>	-9.83.10 <sup>-2</sup>
0.3969	0.3208	997.1	0.6860	-5.31.10 <sup>-7</sup>	-2.21.10 <sup>-1</sup>
0.3259	0.4423	969.7	0.7688	-5.69.10 <sup>-7</sup>	-3.05.10 <sup>-1</sup>
0.3153	0.4604	965.7	0.7849	-6.02.10 <sup>-7</sup>	-3.14.10 <sup>-1</sup>
0.2382	0.5923	933.0	0.9333	-6.58.10 <sup>-7</sup>	-3.45.10 <sup>-1</sup>
0.1887	0.6771	909.5	1.0651	-6.22.10 <sup>-7</sup>	-3.29.10 <sup>-1</sup>
0.1776	0.6962	903.9	1.0980	-6.03.10 <sup>-7</sup>	-3.22.10 <sup>-1</sup>
0.1113	0.8095	868.7	1.3298	-4.67.10 <sup>-7</sup>	-2.45.10 <sup>-1</sup>
0.0522	0.9106	833.9	1.5790	-2.71.10 <sup>-7</sup>	-1.33.10 <sup>-1</sup>
0.0189	0.9677	812.8	1.7361	-1.38.10 <sup>-7</sup>	-5.39.10 <sup>-2</sup>
0.0000	1.0000	799.8	1.8340	0.00	0.00

(continued on next page)

Table 3 (continued)

$X_1$	$X_3$	$\rho / \text{kg/m}^3$	$\eta / \text{mPa}\cdot\text{s}$	$V^E \text{ m}^3/\text{mol}$	$\Delta\eta / \text{mPa}\cdot\text{s}$
$\delta_6 = 2.82580$					
0.7075	0.0000	1176.6	0.600	$-1.56 \cdot 10^{-6}$	$1.10 \cdot 10^{-1}$
0.5982	0.1545	1123.9	0.634	$-8.15 \cdot 10^{-7}$	$-6.40 \cdot 10^{-2}$
0.4896	0.3080	1073.5	0.704	$-5.21 \cdot 10^{-7}$	$-2.00 \cdot 10^{-1}$
0.3949	0.4418	1028.6	0.813	$-4.50 \cdot 10^{-7}$	$-2.71 \cdot 10^{-1}$
0.3033	0.5713	982.2	0.961	$-3.95 \cdot 10^{-7}$	$-2.97 \cdot 10^{-1}$
0.2557	0.6386	956.6	1.053	$-3.52 \cdot 10^{-7}$	$-2.95 \cdot 10^{-1}$
0.2237	0.6839	938.7	1.127	$-3.10 \cdot 10^{-7}$	$-2.82 \cdot 10^{-1}$
0.1916	0.7292	920.3	1.211	$-2.66 \cdot 10^{-7}$	$-2.59 \cdot 10^{-1}$
0.1439	0.7965	892.1	1.341	$-2.04 \cdot 10^{-7}$	$-2.20 \cdot 10^{-1}$
0.0676	0.9045	844.4	1.587	$-8.78 \cdot 10^{-8}$	$-1.19 \cdot 10^{-1}$
0.0000	1.0000	799.8	1.834	0.00	0.00
$\delta_7 = 4.47134$					
0.7928	0.0000	1254.2	0.585	$-1.15 \cdot 10^{-6}$	$8.19 \cdot 10^{-2}$
0.7509	0.0529	1231.3	0.583	$-8.57 \cdot 10^{-7}$	$9.36 \cdot 10^{-3}$
0.6610	0.1662	1184.3	0.613	$-4.71 \cdot 10^{-7}$	$-1.11 \cdot 10^{-1}$
0.5456	0.3118	1125.8	0.703	$-3.29 \cdot 10^{-7}$	$-2.15 \cdot 10^{-1}$
0.4298	0.4579	1065.5	0.850	$-3.39 \cdot 10^{-7}$	$-2.63 \cdot 10^{-1}$
0.3385	0.5731	1015.0	0.999	$-3.31 \cdot 10^{-7}$	$-2.67 \cdot 10^{-1}$
0.2921	0.6316	988.2	1.082	$-3.16 \cdot 10^{-7}$	$-2.62 \cdot 10^{-1}$
0.2605	0.6715	969.5	1.149	$-3.02 \cdot 10^{-7}$	$-2.48 \cdot 10^{-1}$
0.2293	0.7108	950.5	1.216	$-2.67 \cdot 10^{-7}$	$-2.33 \cdot 10^{-1}$
0.1782	0.7753	918.6	1.331	$-2.10 \cdot 10^{-7}$	$-2.04 \cdot 10^{-1}$
0.0830	0.8954	856.4	1.581	$-7.92 \cdot 10^{-8}$	$-1.14 \cdot 10^{-1}$
0.0000	1.0000	799.8	1.834	0.00	0.00

Experimental uncertainties u:  $u(T) = 0.01 \text{ K}$ ,  $u(\rho) = 0.1 \text{ kg}\cdot\text{m}^{-3}$ ,  $u(\eta) = 0.0001 \text{ mPa}\cdot\text{s}$ .

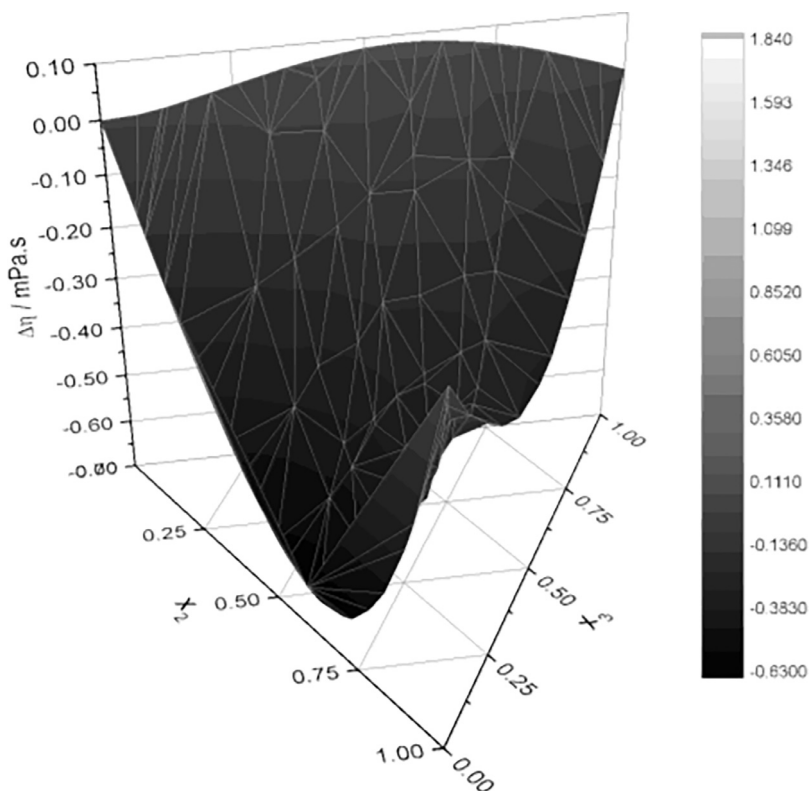


Fig. 6. 3D surface of viscosity deviation  $\Delta\eta$  against molar fractions of chloroform ( $x_1$ ) and dipe ( $x_2$ ) + 1-propanol ( $x_3$ ) at  $(298.15 \pm 0.01) \text{ K}$ .

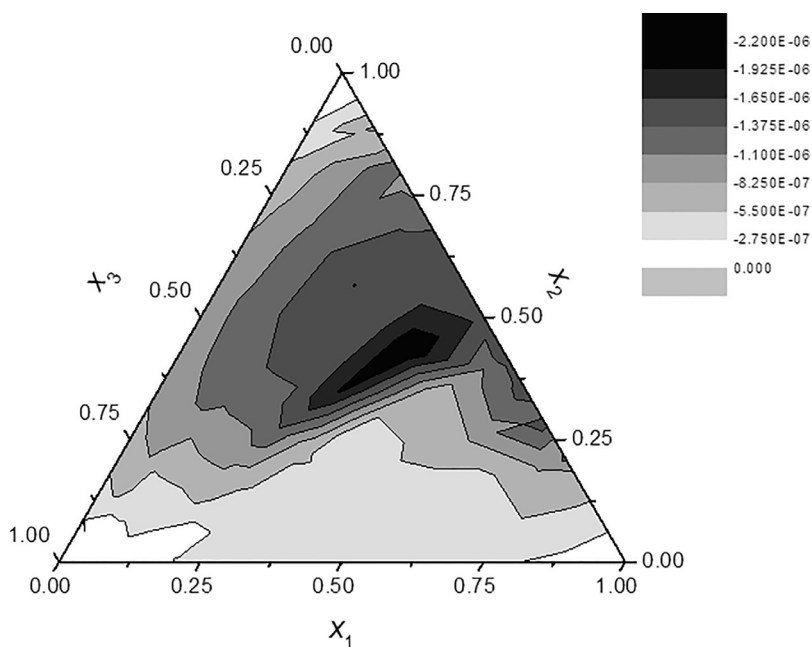


Fig. 7. Contourn lines of excess molar volume  $V^E$  for the [chloroform (1) + dipe(2) + 1-propanol (3)] ternary system at  $(298.15 \pm 0.01)$  K.

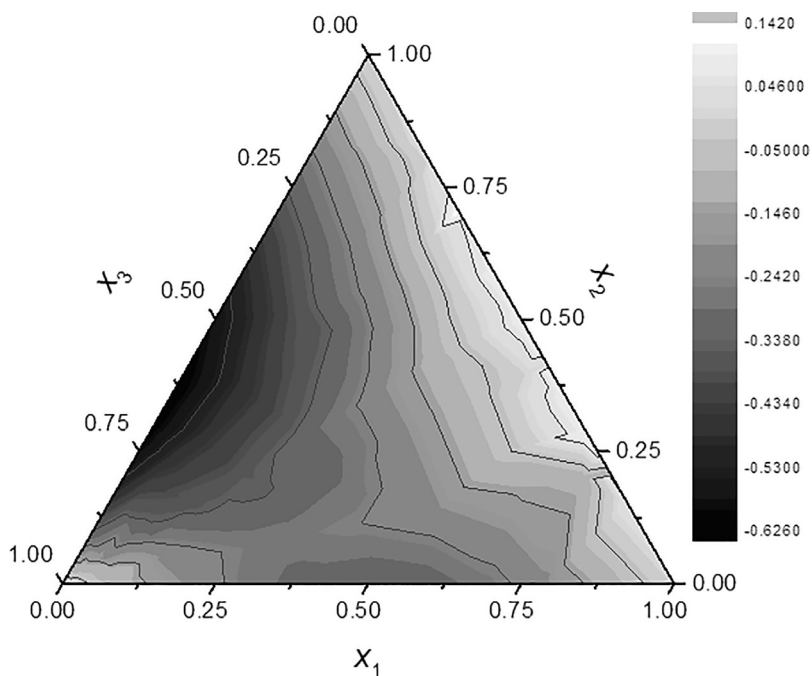


Fig. 8. Contourn lines of viscosity deviation  $\Delta\eta$  for the [chloroform (1) + dipe(2) + 1-propanol (3)] ternary system at  $(298.15 \pm 0.01)$  K.

### 3. Data, value and validation

In Table 1 the measured and literature values of density  $\rho$  and viscosity  $\eta$  of the reagents at  $(298.15 \pm 0.01)$  K were reported.

Scarce data on density or viscosity was found in the literature for the 1-propanol at the temperature of 298.15 K, thus, the data provided in this work is a valuable contribution. The values obtained fit well within the experimental uncertainty.

The experimental values of the density  $\rho$  and viscosity  $\eta$  and the values calculated of the excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for the [chloroform (1) + 1-propanol(3)] binary system at  $(298.15 \pm 0.01)$  K are shown in Table 2.



**Table 4**Parameters  $a_p$  of Eq. 3 and the corresponding standard deviation for the [chloroform (1) + 1-propanol (3)] binary system.

$a_0$	$a_1$	$a_2$	$\sigma$
Chloroform (1) + 1- propanol (3)			
$-1.62 \cdot 10^{-6}$	$-6.7 \cdot 10^{-8}$	$-1.9 \cdot 10^{-7}$	$2 \cdot 10^{-9} \text{m}^3 \cdot \text{mol}^{-1}$
-2.491	-2.015	-0.402	$1 \cdot 10^{-4} \text{mPa} \cdot \text{s}$

**Table 5**Parameters  $B_n$  of Eq. 5 and standard deviations  $\sigma_R$ ,  $\sigma_{N\&T}$  and  $\sigma_{RCT}$  for Eqs. 4, 5 and 7 for [chloroform (1) + DIPE (2)+ 1-propanol (3)] ternary system at 298.15 K.

Parameter	$V^E / \text{m}^3 \cdot \text{mol}^{-1}$	$\Delta\eta / \text{mPa} \cdot \text{s}$
$B_0$	$-1.5871 \cdot 10^{-8}$	-0.03247
$B_1$	$-4.39307 \cdot 10^{-8}$	-0.1542
$B_2$	$-1.22859 \cdot 10^{-7}$	-0.06278
$B_3$	$-2.99683 \cdot 10^{-8}$	0.32455
$B_4$	$3.09256 \cdot 10^{-7}$	0.10224
$B_5$	$3.66017 \cdot 10^{-7}$	0.10537
$B_6$	$1.46658 \cdot 10^{-7}$	-0.21519
$B_7$	$-3.14895 \cdot 10^{-7}$	-0.08222
$B_8$	$-6.38317 \cdot 10^{-7}$	-0.15915
$\sigma_R$	$5 \cdot 10^{-7}$	$4 \cdot 10^{-1}$
$\sigma_{N\&T}$	$6 \cdot 10^{-7}$	$7 \cdot 10^{-1}$
$\sigma_{CT}$	$8 \cdot 10^{-7}$	$5 \cdot 10^{-2}$

Table 3 shows the experimental values of the density  $\rho$  and the viscosity  $\eta$ , and the calculated values for the excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for the [chloroform (1)+DIPE (2)+ 1-propanol (3)] ternary system at  $(298.15 \pm 0.01)$  K.

Experimental determinations were repeated at least three times. Mixtures of any composition are also prepared and their properties are determined experimentally to obtain the total uncertainty of the proposed relationship. Additionally, residual analysis is performed in each case.

Excess thermodynamic functions and deviations of non thermodynamic ones of binary and ternary liquid mixtures are very important for the design of industrial equipment and for the interpretation of the liquid state, particularly when polar components are involved because there exists a possibility of drawing conclusions about the interactions between the components of the mixture.

Numerical values of the coefficients  $a_p$  of Eq. 3 obtained from a least squares analysis of the data for the [chloroform (1)+1-propanol (3)] binary system are listed in Table 4 with standard deviations. The parameters corresponding to the others binary systems have already been published [6,22].

Numerical values of the coefficients  $B_n$  of the Eq. 5, obtained from a least squares analysis [14] of the data for ternary systems are listed in Table 5 with standard deviations ( $\sigma_{N\&T}$ ). Table 5 also shows the standard deviation that is obtained by applying Eq. 4 corresponding to the Radojković ( $\sigma_R$ ) equation and modified version of the Nagata –Tamura equation ( $\sigma_{CT}$ ), Eq. (7).

The results of the adjustment with the Redlich-Kister equation are poor for this ternary system and for this reason they were not included in the table.

#### 4. Conclusions and discussion

Experimental data of density and viscosity are provided for the [chloroform (1)+1-propanol (3)] binary system and [chloroform (1) DIPE (2)+ 1-propanol (3)] ternary system at  $(298.15 \pm 0.01)$  K, and adjustment equations for binary and ternary systems are provided across the range of composition.

The excess molar volume  $V^E$  and viscosity deviation  $\Delta\eta$  for binary systems correlate well within of the experimental error by a Redlich-Kister (Eq. 3) type equation. The ternary excess molar volumes  $V^E$  and viscosity deviation  $\Delta\eta$  correlate well within the experimental error by Nagata and Tamura (Eq. 5) type equation and poorly with the one the Redlich-Kister (Eq. 6) type equation. Also, the ternary excess molar volumes and viscosity deviation  $Y_{123}^E$  were predicted using the Radojković (Eq. 4) equation.

For this ternary system, the prediction using the Radojković equation has a dispersion of the same order as the experimental error and it is less than that corresponding to those obtained with the correlation equations and with the modified version of the Nagata –Tamura equation (Eq. 7).

In the mixture of [chloroform (1)+DIPE (2)] intermolecular bonds appear and therefore the excess molar volume is negative over the full range of composition and with a minimum near to  $x_1 \approx 0.5$ . The viscosity deviation is positive over

the range of composition with a maximum nearest 0.5. For [chloroform (1)+1-propanol (3)] and [DIPE (2)+1-propanol (3)] systems, solvent effect appears which is responsible to break the self-association of 1-propanol. Both systems have a negative excess molar volume and positive viscosity deviation over the entire composition range (see Fig. 1 and Fig. 2), which corroborates the previous statement.

Figs. 3 and 6 show that the molar excess volume is negative, showing remarkable minimum at low concentrations of chloroform and 1-propanol and high of DIPE. The viscosity deviation is negative throughout the composition range, which would imply that the predominant process in this ternary system is the breakage of the self-associations in the 1-propanol.

Figs. 5 and 6 show the 3D graphs of the excess molar volume and the viscosity deviation for the [chloroform (1)+DIPE (2)+1-propanol (3)] ternary system at (298.15±0.01) K. Figs. 7 and 8 show the contours of the excess molar volume and viscosity deviation for this ternary system.

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