



Microstructural study of nanocrystalline pure and doped tin dioxide to be used for resistive gas sensors

M.F. Bianchetti^a, C. Arrieta^b, N.E. Walsöe de Reca^{a,*}

^a CINSO (Solid State Research Dept.) CITEDEF, UNIDEF (MINDEF-CONICET), Juan B. de La Salle 4397, Villa Martelli, B1603 ALO Buenos Aires, Argentina

^b Microelectronics, Thin Films Laboratory – CITEDEF, Juan B. de La Salle 4397, Villa Martelli, B1603 ALO Buenos Aires, Argentina

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ABSTRACT

Nanocrystalline pure and doped SnO₂ have been intensively studied for a long time to build resistive gas sensors. However, it is still useful to synthesize nanopowders with the smallest crystallite size to build devices. A modified gel-combustion method and a novel reactive oxidation process are proposed for nanopowders synthesis and results are compared. Materials have been characterized by XRD, Scherrer equation to evaluate the crystallite size; BET absorption to determine specific area and HRTEM to observe the crystallites (evaluating their mean size and distribution); defects and effect of calcination treatments are also considered. Previous studies have shown that if nano-SnO₂ replaces the conventional microcrystalline-SnO₂ to build resistive gas sensors, sensitivity increases (>30%) and the operation temperature considerably decreases.

A heating and measuring system has been designed for achieving low power consumption and uses pulsed heating operation. This method of electrical control and measurement is operated intermittently, with “heating” and “readout” cycles (readout: signal of sensitive film).

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1. Introduction

Tin dioxide semiconductor (SC) has been used to build gas sensors for many years, exhibiting interesting properties which considerably change as the SnO₂ grain size decreases to nanometric dimension. Pure and doped nano semiconductors were studied and already applied for resistive gas sensors [1–7]. The replacement of the conventional microcrystalline pure or doped SnO₂ by the same material but nanocrystalline to build the gas sensors, has driven to interesting results since the sensor sensitivity increased (30–37%) and the operation temperature (T_{op}) considerably decreased from 350–450 °C to a range: 250–350 °C for nanocrystalline Al-doped SnO₂, and similarly for In doped SnO₂. Fig. 1 or to 180–220 °C for pure nano-SnO₂ [8–10], Fig. 2. The gas detection process is affected by several factors, among them the microstructure. The metallic oxide previously reacts with the air oxygen forming at the SC-surface oxygen adsorbates, (O^- , O_2^- , O^{2-}) [11–13] which play an important role in gas sensing (being the O^- the most active). The adsorbates cover the SC-surface and the grain boundaries and react at the $T_{op} \sim 350$ –450 °C if the sensor is built with microcrystalline

semiconductor. In case of n -type SC metallic oxides, the formation of these adsorbates builds a space-charge region, resulting in an electron-depleted surface layer (space-charge) due to the electron transfer to the adsorbate as follows:



The depth of the space-charge is a function of the surface coverage with the oxygen adsorbates and of the intrinsic electron concentration in the bulk. The resistance of the n -type SC is, in consequence, high because a potential barrier to the electronic conduction is formed at each grain boundary [11]. If the sensor is exposed to a reducing gas (i.e. CO) at the T_{op} , the gas reacts with oxygen adsorbate (O^-) according to:



The oxygen adsorbates are consumed by the subsequent reactions, so that a lower steady-state is established, the potential barrier height decreases and a resistance drop is produced, being the resistance variation the measuring parameter of sensor. A simple schematic model for grain-size affecting the surface resistivity was proposed by Yamazoe et al. [11] concluding that the sensor sensitivity increases as grain size decreases. The sensor sensitivity (S) can be defined as: $S = R_{air}/(R_{air} + R_{gas})$, where: R_{air} is the resistance in air and R_{gas} is the resistance in a gas sample containing a reducing

* Corresponding author. Tel.: +54 11 4709 8158; fax: +54 11 4709 8158.

E-mail addresses: mbian@citedef.gob.ar (M.F. Bianchetti), carrieta@citedef.gob.ar (C. Arrieta), walsoe@citedef.gob.ar (N.E. Walsöe de Reca).

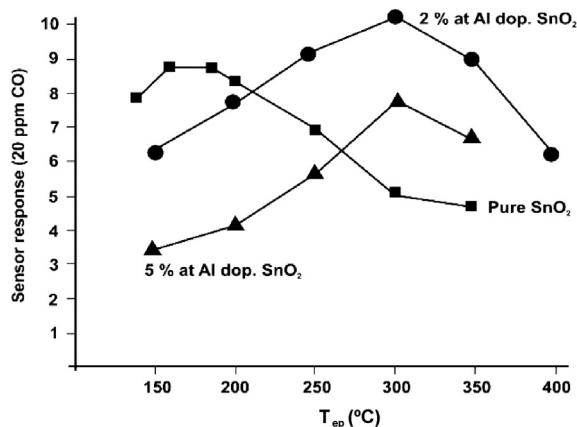


Fig. 1. Sensor response to 20 ppm CO (g) for doped SnO₂ (at%) vs. T_{op} (°C).

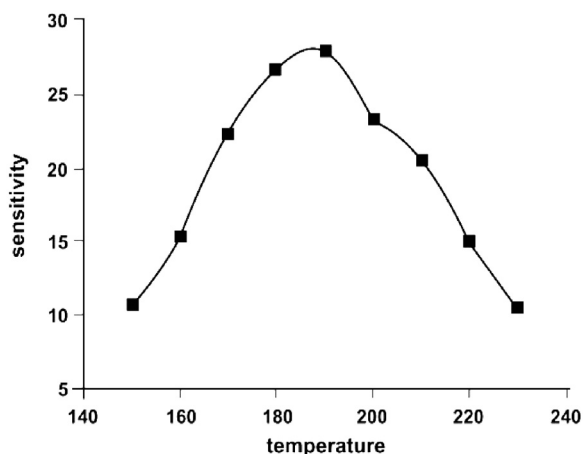


Fig. 2. Sensor sensitivity to 5 ppm H₂ for pure SnO₂ vs. T_{op} (°C).

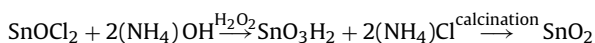
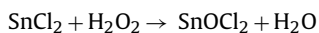
component. The reactivity of the oxygen adsorbates is a function of the type of reducing gas and of sensor temperature.

The aim of this work was to analyze the structure and morphology of pure and doped (with Al or In) nanocrystalline SnO₂ with different crystallite diameters (ϕ), to be applied for gas sensors. Nanomaterials were prepared by gel-combustion [14] and/or by reactive oxidation with H₂O₂ [15] and results of both methods were compared with similar results [7]. Characterization was performed by X-ray diffraction (XRD), Brunauer–Emmer–Teller isotherms (BET) method and High Resolution Transmission Electron Microscopy (HRTEM).

2. Experimental

2.1. Pure SnO₂ synthesis

Pure SnO₂ nanopowders were synthesized by two techniques and results are compared as described in [7]: reactive oxidation with H₂O₂ [15] and modified nitrate–citrate gel combustion [14]. In the first method, the SnCl₂ reacts with H₂O₂ treating afterwards the product with (NH₄)OH in H₂O₂ medium. Stannic acid is produced giving nanopowdered SnO₂ by calcination:



The violent oxidation reaction with H₂O₂ disintegrates the product particles yielding small crystallites with diameters: 2–9 nm.

The *gel-combustion*, fuel-rich synthesis [14] starts with the preparation of a precursor: (aqueous solution with p/a metallic Sn), 70% – HNO₃, CH₃COOH and 25% – NH₄·OH. Citric acid is the organic fuel; [tin/fuel] ratio = 1:6. The pH was increased with (NH₄)OH (approaching to neutrality and keeping the solution homogeneity). The solution is thermally evaporated till turning into a gel. If heating is sustained, gel turns into a dark foam which ignites. The intense combustion of the final stage is due to a highly exothermic redox reaction between the oxidizing nitrate ions and the organic fuel. TGA plots of gellified samples show that gels usually liquefy at ~80°C and ignition starts at ~200–300°C. Combustion usually promotes an ignition not depending on atmospheric oxygen supply, since the foam bubbles are filled either with NH₄NO₃ vapours or NO_x ($1 \leq x \leq 2$) restricting the oxygen access to the bottom of reaction container. Combustion duration is short: usually, half of a minute. Gas liberation promotes the fast disintegration of precursor gel at high temperature causing decomposition. If the oxide contains carbonaceous residues by a fuel surplus, they are removed by calcination and nanometric crystallites (9–15 nm) are produced. Parameters to be fitted are: organic fuel type, combustion temperature and process duration. After the synthesis, the crystallites size and homogeneity, their morphology and the impurities retention during the synthesis process have been evaluated.

2.2. Doped SnO₂ synthesis

The gas sensor to detect hydrogen was built with nanocrystalline pure SnO₂ [9] CO (g) ppm was built with Al-doped nanocrystalline SnO₂ [8] and that for VOCs sensing [10]. The method to prepare the two first materials was gel-combustion using CH₃COOH as fuel and the crystallite size resulted: 2–4 nm. In case of In-doped nanocrystalline SnO₂ [10] the synthesis method consisted in precipitating together p/a SnCl₂·2H₂O and InCl₃, in NH₄NO₃ medium to produce stannic oxo-hydroxide which was intensively oxidized with 30–250 vol H₂O₂ thus obtaining stannic acid as nanocrystalline powder. This solution was precipitated with (NH₄)OH to get an homogeneous compound of stannic acid and indium hydroxide. The resulting crystallite size was ~2–4 nm.

2.3. Characterization of nanomaterials

XRD enabled to identify the material, to evaluate the crystalline structure and to measure crystallites size by application of Scherrer equation; BET measurements were used to determine the specific area and HRTEM, Fig. 3a and b, enabled to observe the crystallites morphology, size and distribution and the calcination temperature effects.

2.4. Sensors building and heating/measuring system

This item is a brief description of functional principle of the sensor gas by direct contact.

In case of using pure or doped nano-SnO₂ to build the sensor and to reduce the power consumption, an innovative heater and measurement device [16], similar to those used for thin film sensors [17], was developed with MEMS Technology (Closed Membrane Type).

The sensor can work in pulsed mode, just as other sensors do, similar to those of the international market. But, differing with them, the sensor described in this work exhibit direct thermal and electrical contact with the sensitive film. This fact enables to reduce a step in the manufacturing process because it is not necessary to isolate the sensitive film and the heater (passivation layer and annealing are not required). This situation improves the efficiency

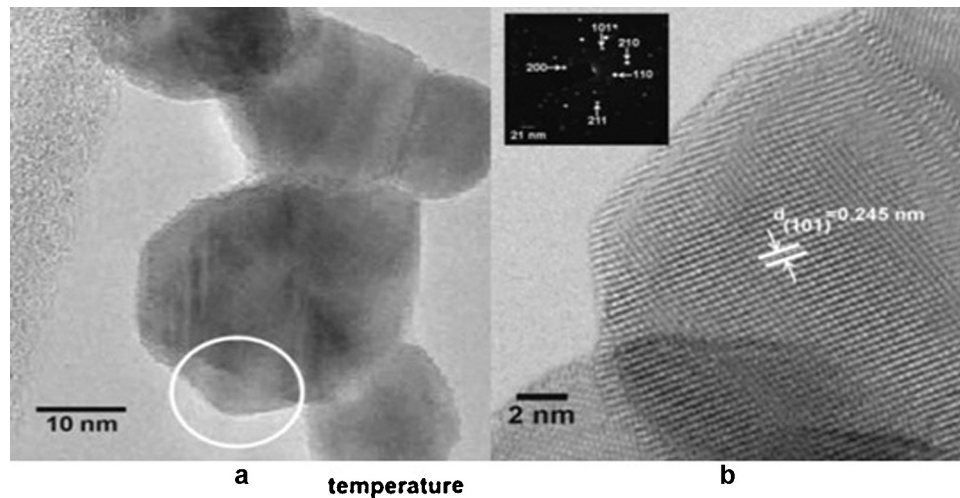


Fig. 3. (a) HRTEM micrograph of SnO_2 crystallites (calcination temperature: 700°C) and (b) Detail of the crystallite shown in (a) (circle) at higher magnification. Defects are observed and twins, dislocations and grain boundaries are shown by arrows.

to transfer heat from the heater to the sensitive film and it also is possible to increase the contact area between the sensitive film and the read-out.

Different gas sensors of SC type, which functioning principle is based on the variation of sensitive film conductivity by interaction with a gas to be detected, requires control of the temperature by a micro-heating device.

The temperature on the platform can be programmed enabling to catalyze a surface chemical reaction, which is electrically measured by the conductivity variation of the sensitive film.

Read out signal, is measured with a trans-impedance amplifier circuit [18] and which is used to evaluate the gas concentration. The micro-heater operation temperature will be confined to the silicon nitride membrane in the active area to perform a periodic heat cleaning (400°C on the sensing layer).

In Fig. 4, it is shown the temperature distribution on the double meander (100 mWatts heating power) by electro-thermal simulation.

The Fig. 5 shows the micro-heater architecture built on a silicon wafer $\langle 100 \rangle$ (thickness $450\ \mu\text{m}$) with a low stress LPCVD Silicon Nitride layer (minor than 200 MPa) and thickness between 0.8 and $1\ \mu\text{m}$

In Fig. 6 it is shown the micro-heater packaged (gold heater and chromium interface layer). Pt was the chosen material for the

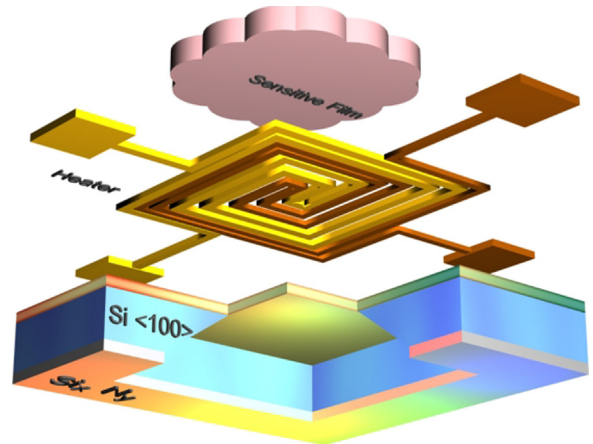


Fig. 5. Scheme of micro heater in the released silicon nitride membrane.

device with an adherent titanium oxide interface (coating) to avoid migration problems on the sensitive film.

The device was fabricated on a micro-machined silicon structure performed with the wet-etching technique (with KOH). The Si_3N_4 layer was used to stop the etching in the micromachining process and to function as a thermal isolation structure [19].

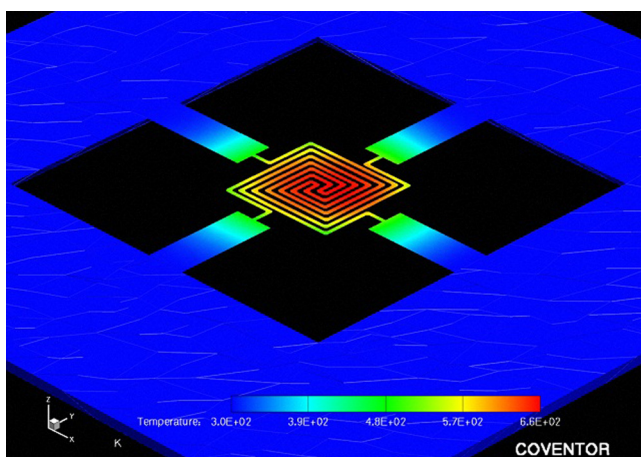


Fig. 4. Temperature distribution on the double meander (100 mWatts heating power) by electro-thermal simulation.

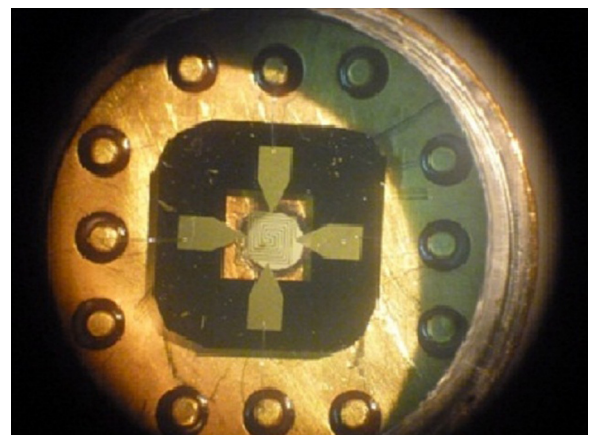


Fig. 6. Sensor on TO-8 package and wire bond details. The active area is surrounded by the transparent membrane which is supported by the outer silicon $\langle 100 \rangle$ frame.

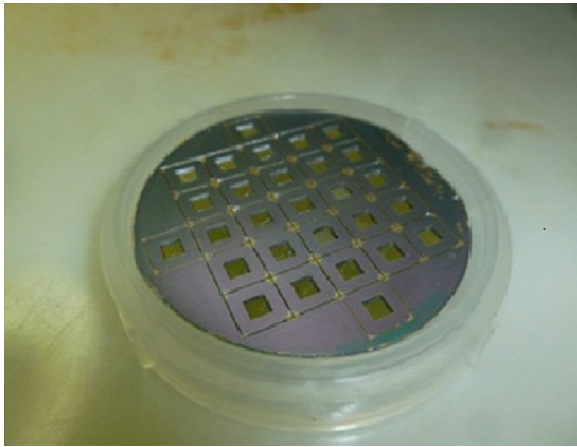


Fig. 7. Micro-machined (back side) of (100) silicon wafer with the closed released membrane.

Fig. 7 shows a (100) silicon wafer with the released membrane, which enables to define the area where the micro-heater is integrated. Due to the membrane low residual stress and small thickness (approximately 1 μm), it is possible to open square windows ($1.5 \times 1.5 \text{ mm}^2$) for the active area. A Au heater (preliminary test) with double meander structure is integrated to SixNy membrane forming the heater-contacts system, working in switched mode. The double meander structure is centred on the released membrane of substrate SixNy. This assembly is used to improve the device thermal isolation and to reduce the power consumption.

This structure is used to heat the sensitive film and to get the read out signal, enabling to improve the thermal and electrical contacts. The sensitive film is printed by standard screen printing technology and annealed before micromachining process.

The double meander structure is used both, as heater and electrical port for the sensitive film (read out mode). The double meander is related to the ad-hoc electronics shown in Fig. 8. A portable device can be built if the arrangement is provided with a microcontroller and its associated electronics (Fig. 9).

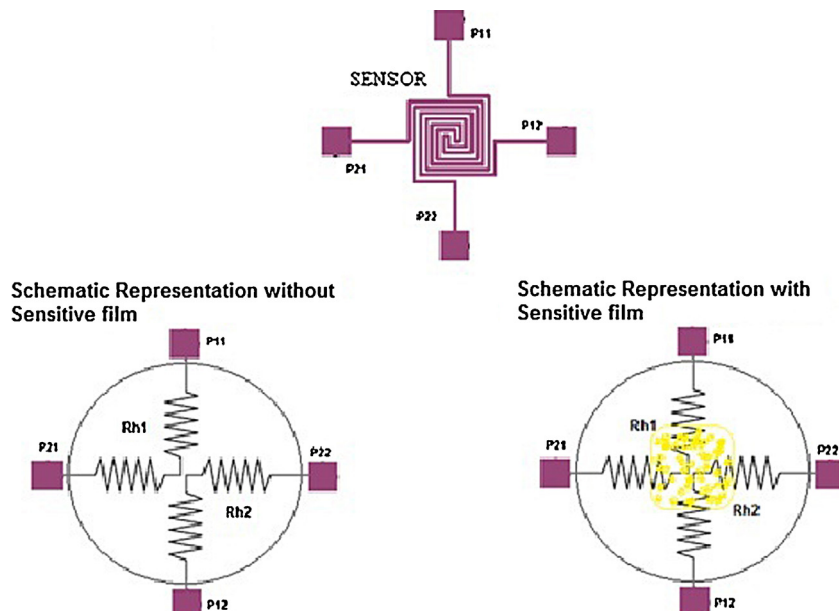


Fig. 8. Double meander detail and schematic representation.

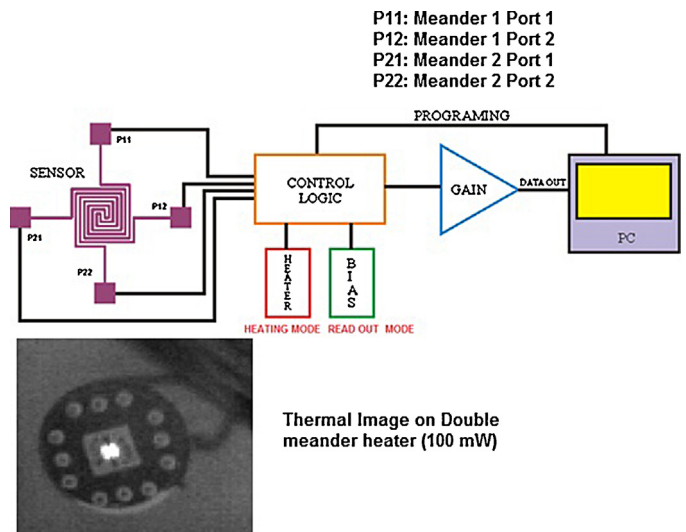


Fig. 9. Scheme of the sensor, electronic controlling switched mode (heating mode and read out mode) and thermal image of micro-heater.

The Data Logger & Calculation block enables the storage in time of the measured conductivity values and their translation to the gas concentration.

The device operating logic is:

- (I) The sensor electrodes are excited, for a period of about some milliseconds, by the heater block which delivers the necessary power for correct functioning (cleaning mode $T=400^\circ\text{C}$ and pre heating for read out mode $T=250^\circ\text{C}$). In this heating stage, the two meanders (resistors), are serial connected. Once removed the heating power, the sensor temperature is maintained during in a fraction of a millisecond (Fig. 10).
- (II) After heating, the control-logic switches the double meander contacts to pick up (Read Out mode with a Interrogation pulse) and enables the bias block to excite the terminals to the adequate polarization levels on the sensitive film, during a few microseconds (Sensitive film temperature is approximately 250°C).

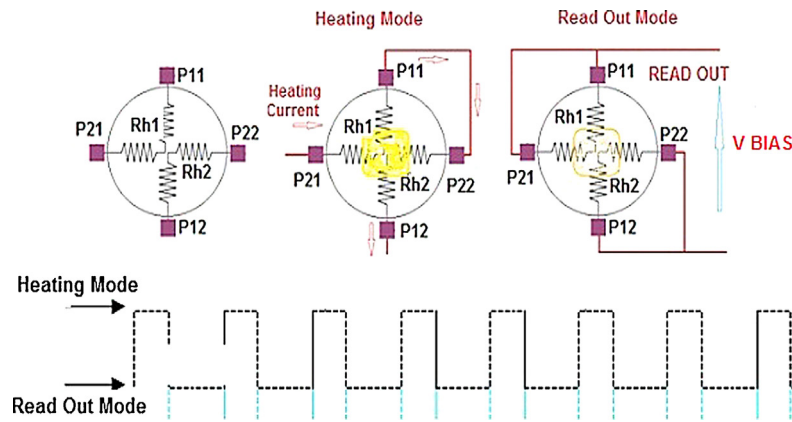


Fig. 10. Schematic representation details, of Heating and Read Out modes.

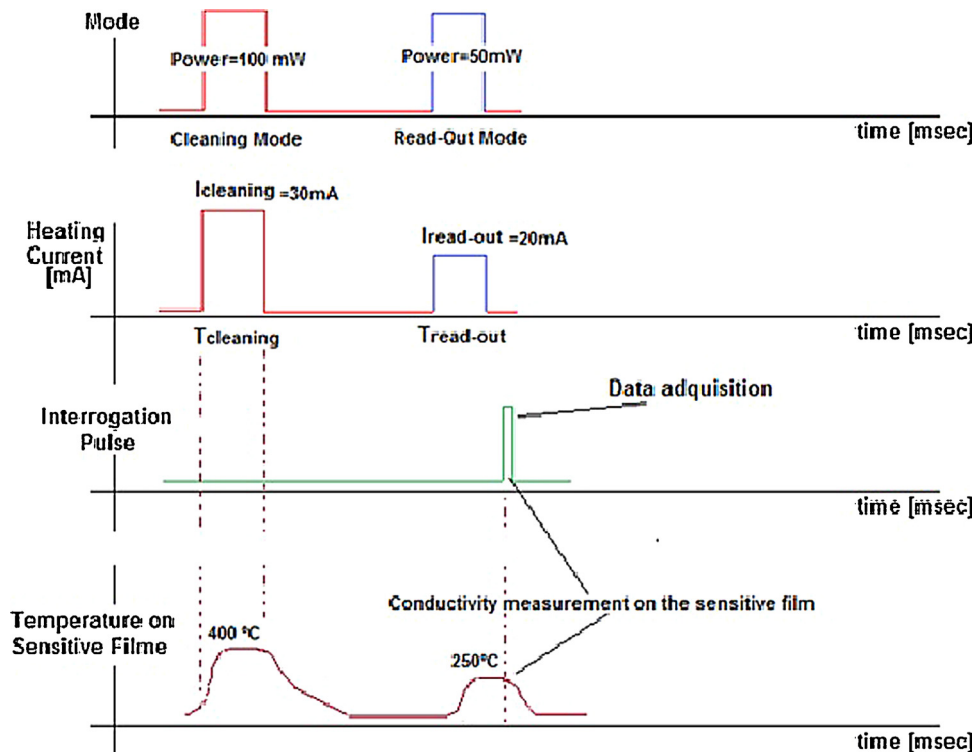


Fig. 11. Timing details to perform the logic operation of device.

(III) The acquired data are stored being repeated the whole process according the programming. Details of timing can be observed in Fig. 11.

3. Conclusions

Pure and Al and In-doped SnO_2 with different crystallite size ($\bar{\phi}$) were synthesized to build resistive gas sensors (to detect H_2 , CO and VOCs) by a gel-combustion method [$\bar{\phi}$ = 9–15 nm] and by a reactive oxidation with H_2O_2 [$\bar{\phi}$ = 2–9 nm]. XRD, BET absorption technique and HRTEM were applied to characterize the structural and morphological properties of SnO_2 . Calcination temperature causes the grain size growth contributing to decrease the specific area. The analysis of XRD spectra for different sized crystallites always enabled to identify the rutile tetragonal phase for doped SnO_2 . HRTEM micrographs have shown that rounded nanoparticles with the smallest grain size were homogeneously distributed and exhibited higher defects density.

Calcination at higher temperatures caused crystallites with larger grain size exhibiting faceted form and considerably lower density of defects. Sensors built with nano- SnO_2 to detect H_2 , showed a sensitivity value ($\sim 35\%$) higher in comparison with that of reference sensors, being the highest sensitivity value and the T_{op} decrease to ~ 180 – 200°C related to the smallest crystallite size. In case of sensors built with pure or doped nano- SnO_2 . Because of their lower T_{op} , a commutation: heater to measurement device was developed to be incorporated to the sensor.

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Biographies

Mario Fidel Bianchetti is a System Analyst graduated at the Buenos Aires University FCEN-UBA (Argentina), 1998. Research Assistant in Physics, Buenos Aires University (Argentina), 2007. He is a Professional of CONICET (National Council for Scientific and Technologic Research) Technicians career. He has published about 40 scientific papers in international and local reviews, two invention patents and numerous reports for local industry. He was designed and manufactured EDM machines for the local and international industry. He is teaching Numerical Calculation at the FCEN – Buenos Aires University (UBA). He has been honoured with an international prize and a national award

Cristian L. Arrieta graduated in Electronic Engineering at National Technological University (Facultad Regional Bs. As.) on 1999. From 1998 he is a researcher in CITEDEF (Institute for Scientific and Technological Research for the Defence). His present research area includes Micro-Electromechanical Systems, Optical Devices and Electronic Circuit engineering. From 1999 he is an Associated Professor and Lecturer at the National Technological University (UTN), he teaches Circuits Theory and Electromagnetics. He has published some scientific papers in international reviews, one invention patent and reports for the local industry.

Noemí E. Walsõe de Reca is a Chemistry doctor graduated at Buenos Aires University (Argentina) in 1966. Post-doctoral Studies: Materials Science in the Technische Hochschule-München (Germany), at the Centre d' Etudes Nucleaires Saclay (France) and at the Université d' Orsay (France). She is a Senior Researcher of CONICET (National Council for Scientific and Technologic Research) career. She is a Member of the National Academy of Sciences ANCEFN (Argentina). Actually, she is a director of CINSO (Solid State Research Centre) CITEDEF and vice-director of UNIDEF (MINDEF-CONICET). She has published about 300 scientific papers in international reviews, 7 chapters of books, 16 invention patents and numerous reports for the local industry. She was a Professor of Physical Metallurgy at the National Technological University (UTN) and at the Faculty of Engineering-Buenos Aires University (UBA). She directed 32 Doctoral Thesis (PhD) in Engineering, Physics, Chemistry and Materials Science and Argentine and foreign fellowship holders' research work. She has been honoured with numerous international and national prizes and awards.